
LITTLE RIVER
LAMPREY RIVER WATERSHED
NEW HAMPSHIRE

MENDUMS POND DAM-BREAK FLOOD ANALYSIS

SEPTEMBER 1984



**US Army Corps
of Engineers**
New England Division

MENDUMS POND DAM
DAM-BREAK FLOOD ANALYSIS

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MENDUMS POND DAM

DAM-BREAK FLOOD ANALYSIS

1. INTRODUCTION AND PURPOSE

This report presents the findings of a dam-break flood analysis performed for Mendums Pond Dam. The dam is owned, operated, and maintained by the New Hampshire Water Resource Board. Included in the report are a description of pertinent features of the dam, the procedure used for the analysis, the assumed dam-break conditions, and the resulting effect on downstream flooded areas. This study was not performed because of any known likelihood of a dam-break at Mendums Pond Dam. Its purpose is to provide quantitative information for emergency planning use.

2. DAM DESCRIPTION

| | |
|--------------------|---------------------------|
| Identification No: | NH00133 |
| Name of Dam: | Mendums Pond Dam |
| Town: | Nottingham |
| County and State: | Rockingham, New Hampshire |
| Stream: | Little River |

Mendums Pond Dam is 31 feet high, averages about 36 feet wide, and is 440 feet long. It is an earthen embankment placed between vertical dry masonry walls, spans the upper reach of the Little River, and is located in east central New Hampshire.

3. PERTINENT DATA

Data is taken from "Phase I Inspection Report" for Mendums Pond Dam dated August 1978.

a. Drainage Area The drainage area consists of 5.4 square miles (3,456 acres) of gently to steeply sloping wooded terrain.

b. Discharge at Damsite

(1) Outlet works (ports) - One lower gate, 2' H x 4' W and Invert Elevation 195' MSL; 2 upper gates, 1.8' H x 1.5' W and Invert Elevation 209' MSL. Total gate capacity at spillway crest - 300 cfs @ 219' MSL.

(2) Spillway capacity at maximum pool elevation -
1010 cfs @ 224.3' MSL.

c. Elevation (ft. above MSL) (Elevations are
relative to assumed spillway elevation; see (5)
below).

(1) Top of dam - the crest varies from 224.3 to
226.4

(2) Test flood pool - 226.3

(3) Recreation pool - 219

(4) Spillway crest - 219

(5) Upstream invert low-level port - 195

(6) Streambed at centerline of main dam - 195

d. Reservoir (miles)

(1) Length of maximum pool - 1.5

(2) Length of recreational pool - 1.5

e. Storage (acre-feet)

(1) Recreational pool - 1,960 (spillway crest)

(2) Top of dam - 3,300

f. Reservoir Surface (acres)

(1) Top of dam (embankment) - 310

(2) Recreation pool - 209

(3) Spillway crest - 209

g. Dam

(1) Type - earthen embankment placed between
upstream and downstream vertical dry masonry
walls.

(2) Length - 440'

(3) Height - 31' (structural height)

(4) Top width - ranges from 24' to 49'

(5) Side slopes - vertical

h. Spillway

(1) Type - Overflow concrete weir, 2' high, with a crest width of 1-1/2'

(2) Length of weir - 25'

(3) Crest elevation - 219' MSL

(4) Gates - None

(5) U/S Channel - Mendums Pond

(6) D/S Channel - The downstream channel is cut in bedrock with a shallow depth of sand, gravel, and boulders on the bottom.

j. Regulating Outlets - Three wooden gates are located over ports in the upstream face of the wall of the control shaft.

4. VALLEY DESCRIPTION

Mendums Pond Dam spans the headwaters of Little River which flows southeasterly for a distance of 7.8 miles to its confluence with the Lamprey River. The river valley is heavily wooded and has a moderate to steep slope of 13 feet/mile. No significant population center is located in the study search.

5. MODEL DESCRIPTION

Mendums Pond dam-break analysis was made using the HEC version, dated November 1981, of the "National Weather Service Dam-Break Flood Forecasting Computer Model", developed by D.L. Fread, Research Hydrologist, Office of Hydrology, National Weather Service, NOAA, Silver Spring, MD 20910. Input for the model consisted of: (a) storage characteristics of the reservoir, (b) selected geometry and duration of the breach development, (c) hydraulic inflows, (d) hydraulic roughness coefficients, and (e) active and inactive flow regions. Based on the input data, the model computes the dam-break outflow hydrograph and routes it downstream. The analysis provides output on the attenuation of the flood stages, and timing of the

flood wave as it progresses downstream.

6. ASSUMED DAM BREAK CONDITIONS

General: The magnitude of a flood resulting from the hypothetical failure of Mendums Pond Dam is a function of many different parameters, including size of breach, initial pool level and storage, rate of breach formation, channel and over bank roughness, and antecedent flow conditions. Engineering assumptions of conditions which could be reasonably expected to exist prior to a failure of Goose Pond Dam and used in the analysis are presented below:

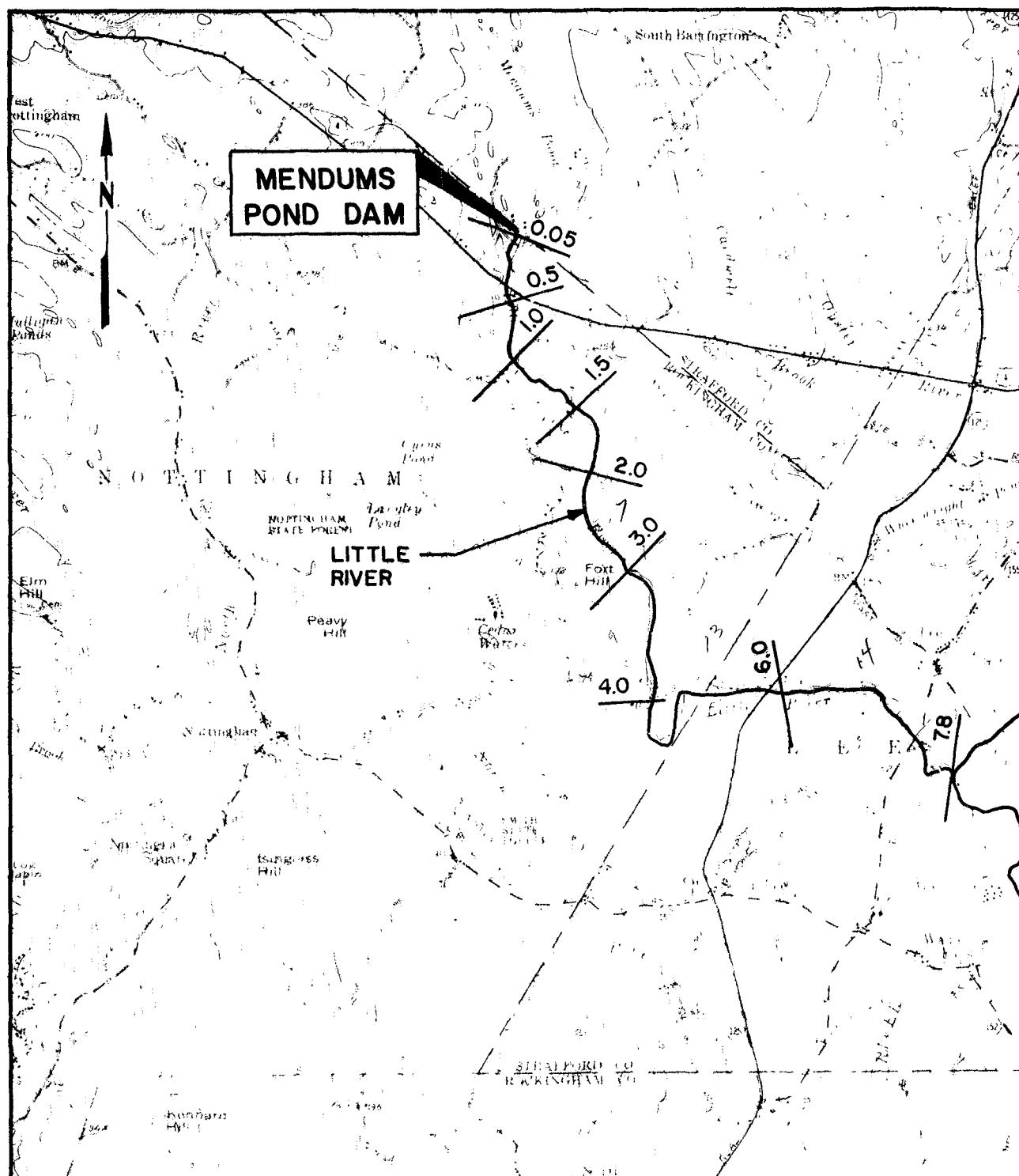
- a. Initial Pool Level 223 feet NGVD, 4.0 feet above top of flashboards
- b. Reservoir Inflow Estimated flood of record = 675 cfs
- c. Breach Invert 195.0 feet NGVD
- d. Breach Base Width 90 feet, trapezoidal side slopes 1V: 0.5H
- e. Time to Complete Formation of Breach 1 hour
- f. Downstream Channel Roughness Manning's "n" = .040 to .140
- g. Pre-Breach River Flows The pre-breath river flow was assumed equal to the flood of record which was estimated by using a cfs/square miles value based upon similar drainage area. Inflow to Mendums Pond was 675 cfs.

7. RESULTS

The resulting peak stage flood profiles are shown on plate 2 and 3. Because of the scarcity of good topographic mapping in the area, profiles are shown in feet above normal summertime (July-August) low water (NLW). Users of the information can establish depth of flooding at particular properties by establishing its relative elevation with respect to the adjacent stream level. Variations in depth above NLW progressing downstream is attributable to changes in natural stream hydraulic capacity, as well as changes in peak discharge.

The peak dam-break discharge from Mendums Pond Dam is 35,650 cfs producing a rise of approximately 20.0 feet above the NLW river depth at a point .05 miles downstream from the dam. At a distance of 6.0 miles below the dam, peak discharge is 21,950 cfs and the rise over NLW stage would be about 14.3 feet. Peak discharge, stage, and timing for three stations downstream from Mendums Pond Dam are shown on plate 4. The stations are located .05, 1.5, and 6.0 miles downstream of the dam.

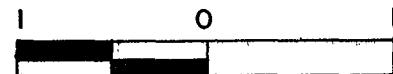
The input data file is in Appendix A, while Appendix B contains the output file.



MAP BASED UPON U.S.G.S.
MT. PAWTUCKAWAY, N.H. QUADRANGLE
1957

CROSS-SECTION LOCATION IN
MILES BELOW DAM

SCALE IN MILES

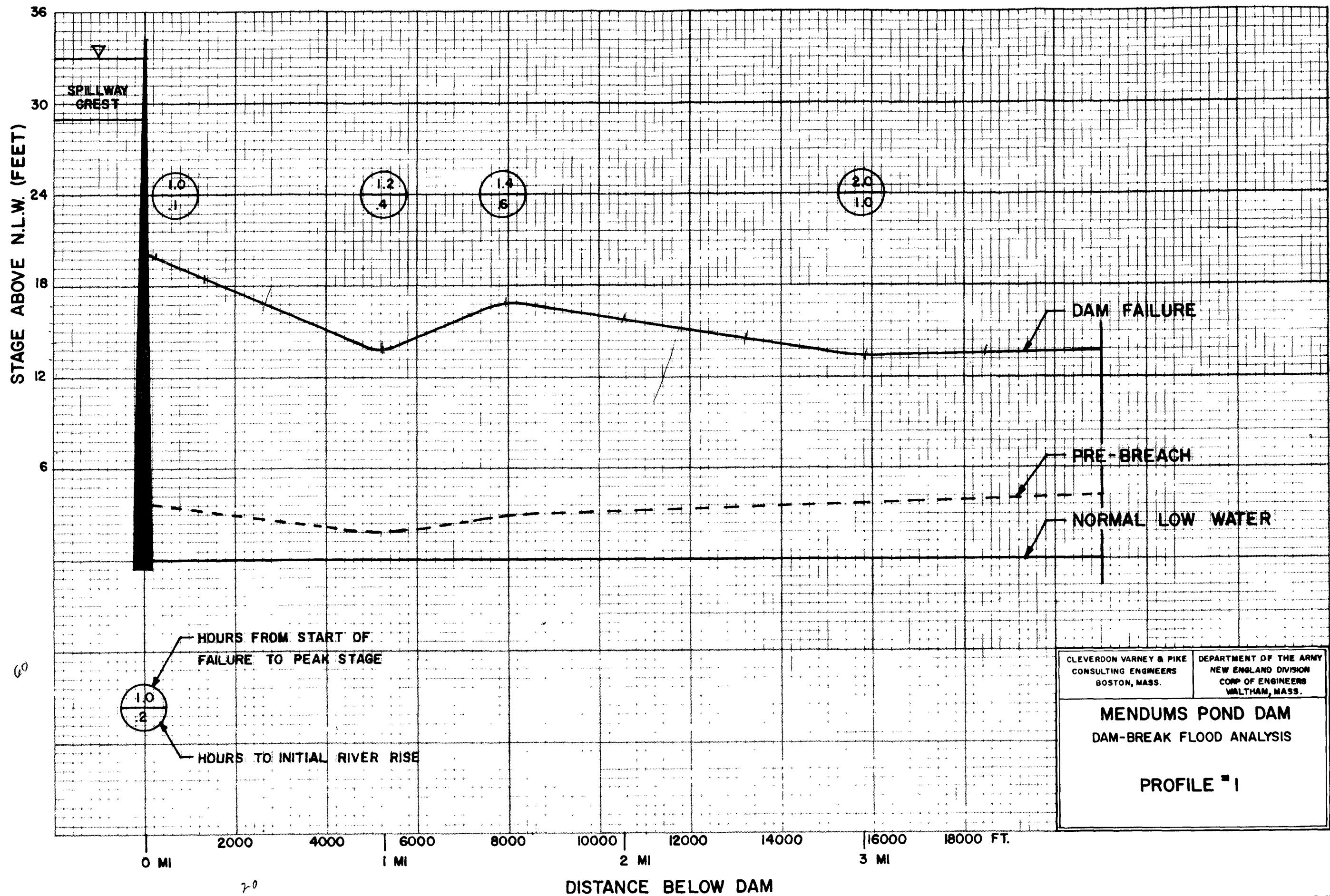


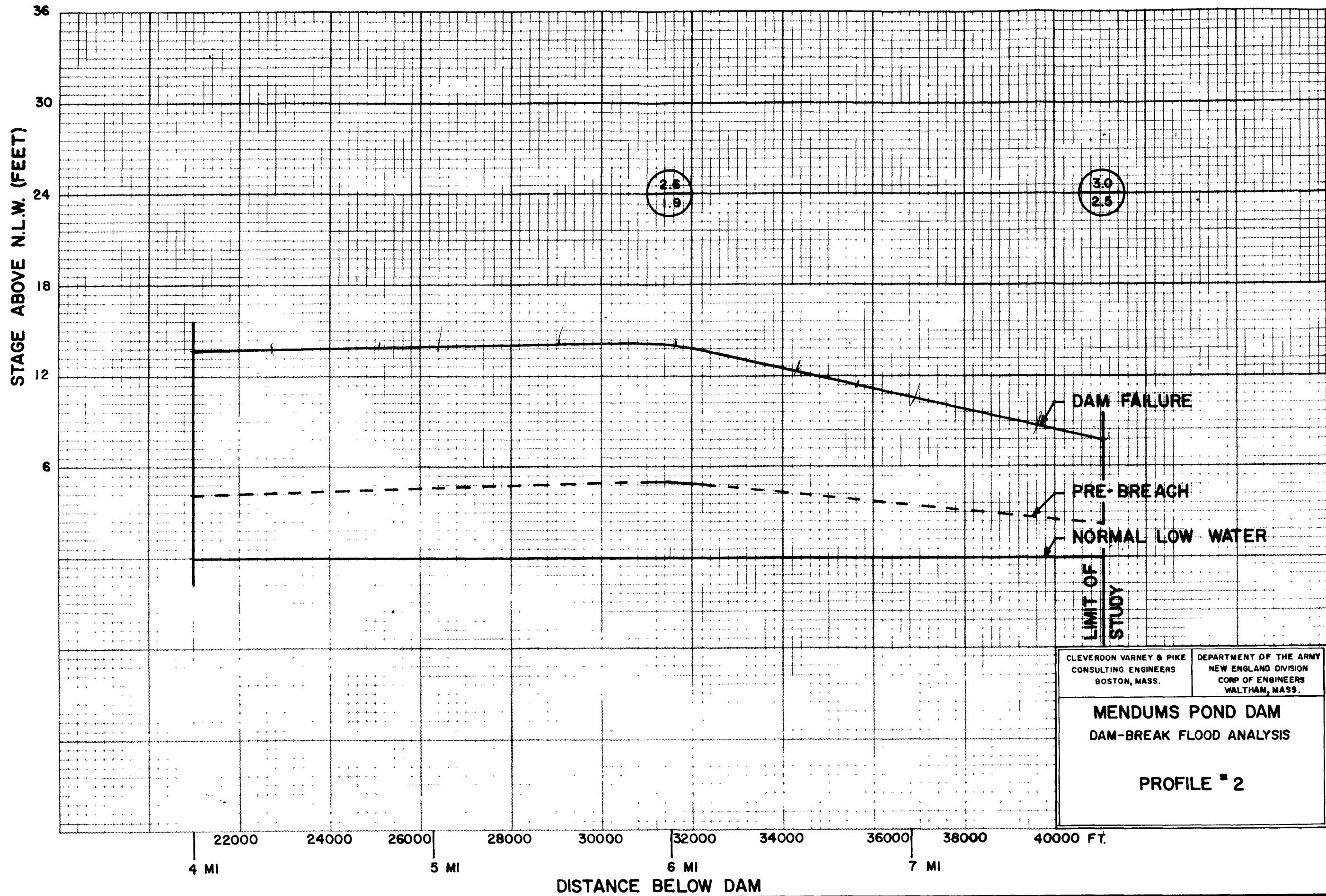
CLEVERDON VARNEY & PIKE
CONSULTING ENGINEERS
BOSTON, MASS.

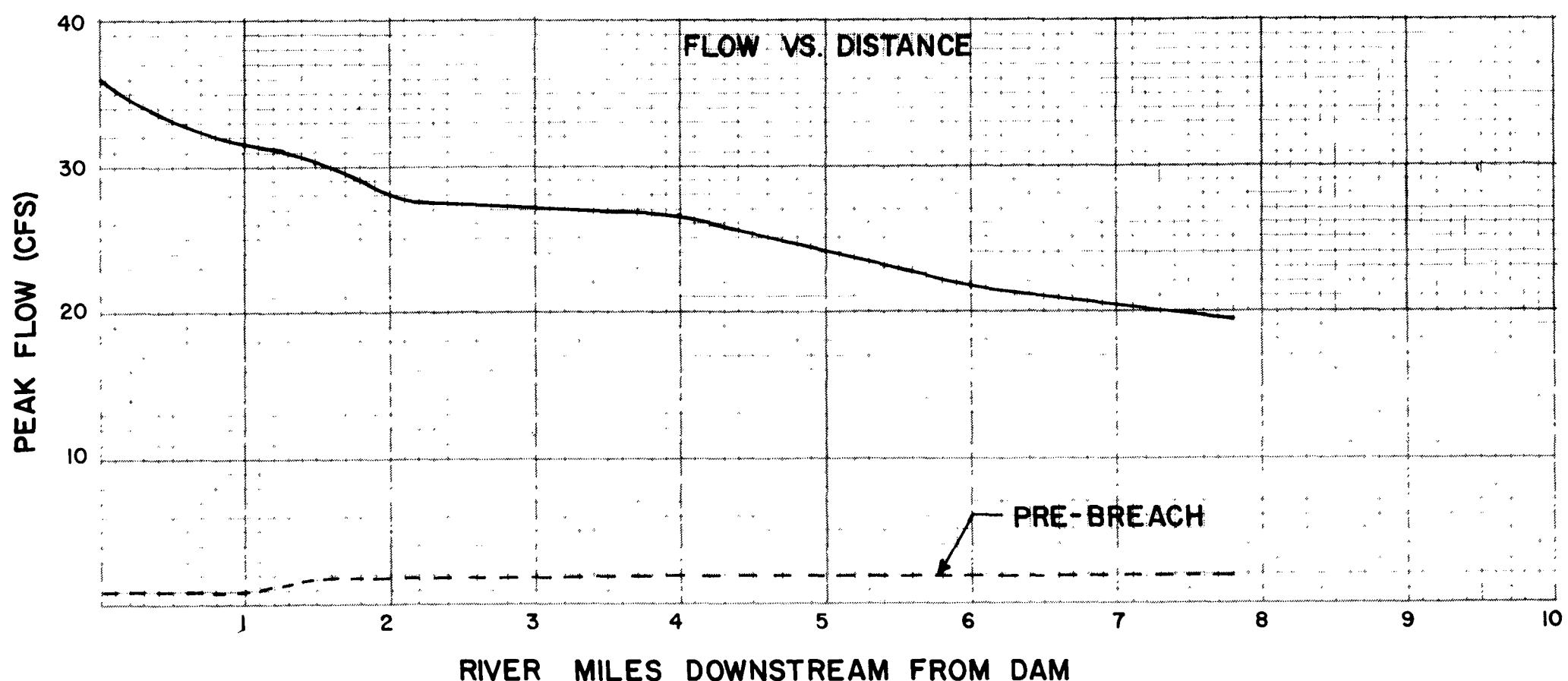
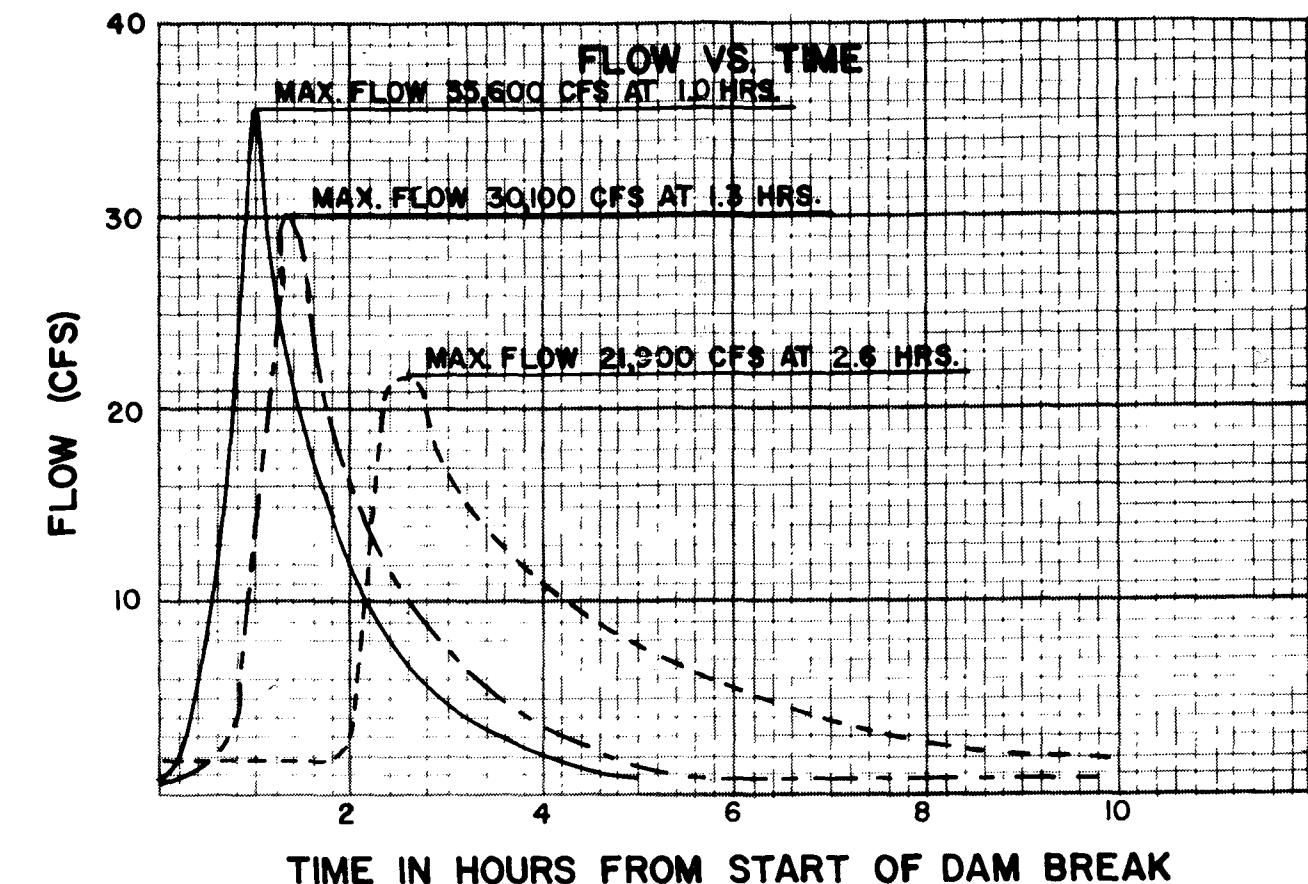
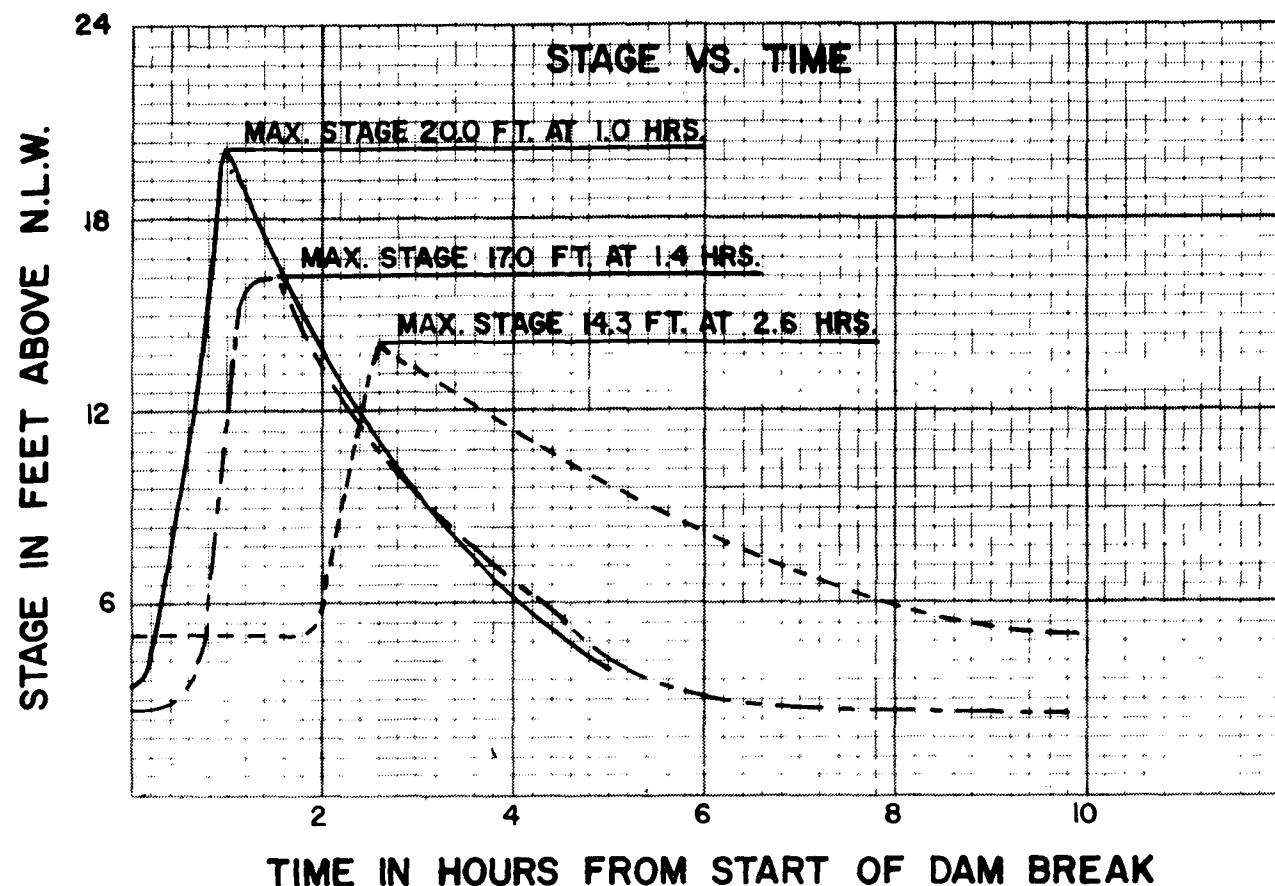
DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION
CORP OF ENGINEERS
WALTHAM, MASS.

**MENDUMS POND DAM
DAM BREAK FLOOD ANALYSIS**

INDEX MAP







NLW DATUM (FT. NGVD)

STA. 1 RM. 0.05 = 190 ~~20.0~~ 210.03
 STA. 2 RM. 1.50 = 157 ~~17.0~~ 113.96
 STA. 3 RM. 6.00 = 111 ~~14.3~~ 126.27

| | |
|--|---|
| CLEVERDON VARNEY & PIKE CONSULTING ENGINEERS BOSTON, MASS. | DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION CORP OF ENGINEERS WALTHAM, MASS. |
|--|---|

MENDUMS POND DAM
DAM-BREAK FLOOD ANALYSIS
BASE FLOOD DISCHARGES
STAGES & TIMING

*HECFORMAT
 *ECHO
 *FORMATTED
 *10FIELDS
 *COMPOSITE
 ID MENDUMS POND DAM
 ID MENDUMS POND
 ID G. MERCER
 ID C.V.&P ENGS.
 ID BOSTON, MA
 IO 1 10 10
 1P 3 1
 QI 675
 SN MENDUMS POND
 SE 224.3 219 195
 SA 310 209 50
 DN MENDUMS DAM
 DD 224.3 219 0 223 10 .06 195
 DB 1 223 90 195 .5
 DO 0 100 0 10
 RN REACH 1
 RG 1 3 4 6 8 9
 RC 0.0 0 0.0 0.0
 XI 0.05
 XE 189 197 205 212 219 226 233 240
 XC 20 200 515 614 742 806 869 933
 XO 0 174 0 0 0 0 0 0
 NC .045 .060 .070 .080 .090 .100 .110 .120
 XI 0.5
 XE 183 192 200 208 216 224 232 240
 XC 30 200 680 1032 1384 1872 1800 2400
 XO 0 174 0 0 0 0 696 720
 NC .045 .060 .070 .080 .090 .100 .110 .120
 XI 1.0
 XE 175 181 188 194 201 207 214 220
 XC 30 282 429 577 725 883 1041 1200
 NC .045 .060 .070 .080 .090 .100 .110 .120
 XI 1.5
 XE 156 163 170 176 182 188 194 200
 XC 28 295 680 1037 1323 1449 1527 1571
 NC .045 .060 .070 .080 .090 .100 .110 .120
 XI 2.0
 XE 151 158 165 172 179 186 193 200
 XC 50 333 610 885 1160 1260 1330 1400
 NC .045 .060 .070 .080 .090 .100 .110 .120
 QN 2.0 LOCAL INFLOW
 QL 1125
 XI 3.0
 XE 143 152 160 168 176 184 192 200
 XC 30 510 937 1186 1435 1664 1872 2080
 NC .035 .045 .050 .060 .070 .080 .090 .100
 XI 4.0
 XE 135 141 148 154 161 167 174 180
 XC 30 237 702 878 1081 1621 2160 2700
 XO 0 300 0 0 0 0 0 0

| | | | | | | | | |
|----|------|------|------|------|------|------|------|------|
| NC | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |
| XI | 6.0 | | | | | | 0.25 | |
| XE | 111 | 118 | 125 | 132 | 139 | 146 | 153 | 160 |
| XC | 10 | 135 | 443 | 567 | 616 | 756 | 780 | 804 |
| NC | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |
| XI | 7.8 | | | | | | | |
| XE | 75 | 81 | 88 | 94 | 101 | 107 | 114 | 120 |
| XC | 50 | 500 | 900 | 1200 | 1300 | 1500 | 1600 | 1700 |
| XO | 0 | 588 | 577 | 512 | 612 | 728 | 940 | 900 |
| NC | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |
| ZZ | | | | | | | | |

| CM | ... | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |
|----------|-------|--------|---------|--------|--------|-------|---------|--------|------|
| SECT NO. | X5(I) | RIVRMI | FSTG(I) | XSL(I) | XSR(I) | YD(I) | DXM(I) | FKC(I) | |
| c | 7.6 | | | | | | 1000000 | | |
| HE | ... | 75 | 81 | 88 | 94 | 101 | 107 | 114 | 120 |
| BS | ... | 50 | 500 | 900 | 1200 | 1300 | 1500 | 1600 | 1700 |
| BSE | ... | 0 | 588 | 577 | 512 | 612 | 728 | 940 | 900 |

PROGRAM DAMBRK---VERSION-A-01/30/82

ANALYSIS OF THE DOWNSTREAM FLOOD HYDROGRAPH

PRODUCED BY THE DAM BREAK OF

MENDUMS POND DAM

ON

MENDUMS POND

ANALYSIS BY

G. MERCER
C.V.&F ENGE.
BOSTON, MA

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 SILVER SPRING, MARYLAND 20910

 *** SUMMARY OF INPUT DATA ***

INPUT CONTROL PARAMETERS FOR MENDUM POND DAM

| PARAMETER | VARIABLE | VALUE |
|--|----------|-------|
| NUMBER OF DYNAMIC ROUTING REACHES | KRN | 1 |
| TYPE OF RESERVOIR ROUTINE | KUJ | 0 |
| MULTIPLE DAM INDICATOR | MULDAM | 0 |
| PRINTING INSTRUCTIONS FOR INPUT SUMMARY | KDMP | 0 |
| NO. OF RESERVOIR INFLOW HYDROGRAPH POINTS | JTEH | 1 |
| INTERVAL OF CROSS-SECTION INFO PRINTED OUT WHEN JNK=1-NPRT | | 0 |
| ELLIPTIC-PLAIN MODEL PARAMETER | KFLP | 0 |
| LANDELIDE PARAMETER | KSL | 0 |

MENDUM POND DAM RESERVOIR

TABLE OF ELEVATION VS SURFACE AREA

| SURFACE AREA (ACRES) SA(ACR) | ELEVATION (FT) HSA(FT) |
|---------------------------------|---------------------------|
|---------------------------------|---------------------------|

| | |
|-------|--------|
| 310.0 | 224.30 |
| 170.0 | 219.00 |
| 50.0 | 195.00 |
| 0.0 | 0.00 |
| 0.0 | 0.00 |
| 0.0 | 0.00 |

0.0

0.00

MENDUME POND DAM RESERVOIR AND BREACH PARAMETERS

| PARAMETER | UNITS | VARIABLE | VALUE |
|--|-------|----------|--------|
| <hr/> | | | |
| LENGTH OF RESERVOIR | MI | RLEN | 0.00 |
| ELEVATION OF WATER SURFACE | FT | YC | 213.00 |
| SIDE SLOPE OF BREACH | | Z | .50 |
| ELEVATION OF BOTTOM OF BREACH | FT | YBMIN | 195.00 |
| WIDTH OF BASE OF BREACH | FT | BR | 90.00 |
| TIME TO MAXIMUM BREACH SIZE | HR | TFH | 1.00 |
| ELEVATION (MSL) OF BOTTOM OF DAM | FT | DATUM | 195.00 |
| VOLUME-SURFACE AREA PARAMETER | | VOL | 0.00 |
| <hr/> | | | |
| ELEVATION OF WATER WHEN BREACHED | FT | HF | 213.00 |
| ELEVATION OF TOP OF DAM | FT | HD | 214.30 |
| ELEVATION OF UNCONTROLLED SPILLWAY CREST | FT | HSP | 219.00 |
| ELEVATION OF CENTER OF GATE OPENINGS | FT | HGT | 0.00 |
| DISCHARGE COEF. FOR UNCONTROLLED SPILLWAY | CS | 100.00 | |
| <hr/> | | | |
| DISCHARGE COEF. FOR GATE FLOW | CG | 0.00 | |
| DISCHARGE COEF. FOR UNCONTROLLED WEIR FLOW | CPW | 0.00 | |
| DISCHARGE THRU TURBINES | CFS | 0.00 | |

DHF (INTERVAL BETWEEN INPUT HYDROGRAPH ORDINATES) = 10.00 HRS.

TEH (TIME AT WHICH COMPUTATIONS TERMINATE) = 10.0000 HRS.

=75.02

TIME OF INFLOW HYDROGRAPH ORDINATES

0.0000

CROSS-SECTIONAL PARAMETERS FOR MENDUMS POND
BELOW MENDUMS POND DAM

| PARAMETER | VARIABLE | VALUE |
|---|----------|-------|
| NUMBER OF CROSS-SECTIONS | NS | 9 |
| MAXIMUM NUMBER OF TOP WIDTHS | NCS | 6 |
| NUMBER OF CROSS-SECTIONAL HYDROGRAPHS TO PLOT | NTT | 6 |
| TYPE OF OUTPUT OTHER THAN HYDROGRAPH PLOTS | JNK | 1 |
| CROSS-SECTIONAL SMOOTHING PARAMETER | KSA | 0 |
| DOWNTSTREAM SUPERCRITICAL OR NOT | NSUPC | 0 |
| NO. OF LATERAL INFLOW HYDROGRAPHS | LQ | 1 |
| NO. OF POINTS IN GATE CONTROL CURVE | KCG | 0 |

NUMBER OF CROSS-SECTION WHERE HYDROGRAPH DESIRED
(MAX NUMBER OF HYDROGRAPHS = 6)

1 2 3 4 5 6 7

CROSS-SECTIONAL VARIABLES FOR MENDUMS POND
BELOW MENDUMS POND DAM

| PARAMETER | UNITS | VARIABLE |
|---|-------|----------|
| LOCATION OF CROSS-SECTION | MI | XE(I) |
| ELEVATION (MSL) OF FLOODING AT CROSS-SECTION FT | FT | FSTG(I) |
| ELEV CORRESPONDING TO EACH TOP WIDTH | FT | HE(K,I) |

WIDE CORRESPONDING EACH ELEV
(ACTIVE FLOW PORTION)
TOP WIDTH CORRESPONDING TO EACH ELEV
(OFF-CHANNEL PORTION)

FT BSS(K,I)

SURFACE AREA CORRESPONDING TO EACH ELEV
(ACTIVE FLOW PORTION)
SURFACE AREA CORRESPONDING TO EACH ELEV
(OFF-CHANNEL PORTION)

ACRES DSA(K,I)

ACRES SSA(K,I)

NUMBER OF CROSE-SECTION
NUMBER OF ELEVATION LEVEL

K

CROSS-SECTION NUMBER 1

XE(I) = .050 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

HS ... 189.0 197.0 205.0 212.0 219.0 226.0 233.0 240.0

BS ... 20.0 200.0 515.0 614.0 742.0 806.0 869.0 933.0

BSS ... 0.0 174.0 0.0 0.0 0.0 0.0 0.0 0.0

B-5

CROSE-SECTION NUMBER 2

XE(I) = .500 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

HS ... 163.0 191.0 200.0 208.0 216.0 224.0 232.0 240.0

BS ... 30.0 200.0 500.0 1000.0 1384.0 1872.0 1800.0 2400.0

BSS ... 0.0 174.0 0.0 0.0 0.0 0.0 0.0 0.0

CROSS-SECTION NUMBER 3

XE(I) = 1.000 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

HS ... 175.0 181.0 188.0 194.0 201.0 207.0 214.0 220.0

BS ... 30.0 282.0 429.0 577.0 725.0 823.0 1041.0 1200.0

47-1011

B-6

CROSS-SECTION NUMBER 4

X5(I) = 1.500 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

| | | | | | | | | |
|---------|-------|-------|-------|--------|--------|--------|--------|--------|
| HS ... | 15e.0 | 1e3.0 | 170.0 | .76.0 | 182.0 | 188.0 | 194.0 | 200.0 |
| SE ... | 26.0 | 295.0 | 680.0 | 1037.0 | 1323.0 | 1446.0 | 1527.0 | 1571.0 |
| BSE ... | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

CROSS-SECTION NUMBER 5

X5(I) = 1.000 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

| | | | | | | | | |
|---------|-------|-------|-------|-------|--------|--------|--------|--------|
| HS ... | 151.0 | 156.0 | 165.0 | 172.0 | 179.0 | 186.0 | 193.0 | 200.0 |
| SE ... | 50.0 | 333.0 | 510.0 | 885.0 | 1160.0 | 1260.0 | 1330.0 | 1400.0 |
| BSE ... | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

CROSS-SECTION NUMBER 6

X5(I) = 3.000 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

| | | | | | | | | |
|---------|-------|-------|-------|--------|--------|--------|--------|--------|
| HS ... | 143.0 | 152.0 | 160.0 | 168.0 | 176.0 | 184.0 | 191.0 | 200.0 |
| SE ... | 30.0 | 510.0 | 937.0 | 1186.0 | 1435.0 | 1664.0 | 1872.0 | 2080.0 |
| BSE ... | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

CROSS-SECTION NUMBER 7

X5(I) = 4.000 FSTG(I) = 0.00 XSL(I) = 0.0 XSR(I) = 0.0

| | | | | | | | | |
|---------|-------|-------|-------|-------|--------|--------|--------|--------|
| HS ... | 125.0 | 141.0 | 148.0 | 154.0 | 161.0 | 167.0 | 174.0 | 180.0 |
| BS ... | 30.0 | 137.0 | 701.0 | 676.0 | 1081.0 | 1621.0 | 2160.0 | 2700.0 |
| BSS ... | 0.0 | 300.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

CROSS-SECTION NUMBER E

| | XSE(I) = 6.000 | FSEG(I) = 0.00 | XSL(I) = 0.0 | XSR(I) = 0.0 | | | | |
|---------|----------------|----------------|--------------|--------------|-------|-------|-------|-------|
| HS ... | 111.0 | 118.0 | 125.0 | 132.0 | 139.0 | 146.0 | 153.0 | 160.0 |
| BS ... | 10.0 | 125.0 | 443.0 | 567.0 | 618.0 | 756.0 | 780.0 | 804.0 |
| BSS ... | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

CROSS-SECTION NUMBER F

| | XSE(I) = 7.900 | FSEG(I) = 0.00 | XSL(I) = 0.0 | XSR(I) = 0.0 | | | | |
|---------|----------------|----------------|--------------|--------------|--------|--------|--------|--------|
| HS ... | 75.0 | 81.0 | 88.0 | 94.0 | 101.0 | 107.0 | 114.0 | 120.0 |
| BS ... | 50.0 | 500.0 | 900.0 | 1200.0 | 1300.0 | 1500.0 | 1600.0 | 1700.0 |
| BSS ... | 0.0 | 585.0 | 577.0 | 511.0 | 612.0 | 725.0 | 840.0 | 902.0 |

MANNING N ROUGHNESS COEFFICIENTS FOR THE GIVEN REACHES
(CM(N,I), N=1..NCS) WHERE I = REACH NUMBER

REACH 1045 .060 .070 .080 .090 .100 .110 .120

REACH 2045 .060 .070 .080 .090 .100 .110 .120

REACH 3045 .060 .070 .080 .090 .100 .110 .120

| | | | | | | | | | | |
|-------|---|-----|------|------|------|------|------|------|------|------|
| REACH | 4 | ... | .045 | .060 | .070 | .080 | .090 | .100 | .110 | .120 |
| REACH | 5 | ... | .045 | .060 | .070 | .080 | .090 | .100 | .110 | .120 |
| REACH | 6 | ... | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |
| REACH | 7 | ... | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |
| REACH | 8 | ... | .035 | .045 | .050 | .060 | .070 | .080 | .090 | .100 |

CROSS-SECTIONAL VARIABLES FOR MENDUMS POND
BELOW MENDUMS POND DAM

| PARAMETER | UNITS | VARIABLE |
|-----------|-------|----------|
|-----------|-------|----------|

| | | |
|--|----|-------|
| MINIMUM COMPUTATIONAL DISTANCE USED BETWEEN CROSS-SECTIONS | MI | DXM/I |
| CONTRACTION - EXPANSION COEFFICIENTS BETWEEN CROSS-SECTIONS | | EKC/I |

| | | |
|--------------|-------|-------|
| REACH NUMBER | DXM/I | EKC/I |
|--------------|-------|-------|

| | | |
|---|------|-------|
| 1 | .100 | 0.000 |
| 2 | .102 | 0.000 |
| 3 | .100 | 0.000 |
| 4 | .100 | 0.000 |
| 5 | .100 | 0.000 |
| 6 | .150 | 0.000 |
| 7 | .200 | 0.000 |
| 8 | .250 | 0.000 |

DOWNSTREAM FLOW PARAMETERS FOR MENDUMS POND
BELOW MENDUMS POND DAM

| PARAMETER | UNITS | VARIABLE | VALUE |
|--|--------|----------|--------|
| MAX DISCHARGE AT DOWNSTREAM EXTREMITY | CFS | QMAXD | 0.0 |
| MAY LATERAL OUTFLOW PRODUCING LOSSES | CFS/FT | QLL | 0.000 |
| INITIAL SIZE OF TIME STEP | 4F | DTHM | 0.0000 |
| INITIAL WATER SURFACE ELEVATION DOWNSTREAM | FT | YDN | 0.00 |
| SLOPE OF CHANNEL DOWNSTREAM OF DAM | FT/MI | SOM | 10.00 |
| THETA WEIGHTING FACTOR | | THETA | 0.00 |
| CONVERGENCE CRITERION FOR STAGE | FT | EPSY | 0.000 |
| TIME AT WHICH DAM STARTS TO FAIL | 4F | TFJ | 0.00 |

LATERAL INFLOW REACH NUMBER

LQX(I)

5

(OL(L, 1 ,L=1,ITER
1125.

*** SUMMARY OF OUTPUT DATA ***

| SLOPE PROFILE | | | | | | | | | | ELEV FEET | MILE | |
|---------------|---------|----|-----|-----|-----|-----|-----|-----|-----|--------------|------|----------|
| | | | | | | | | | | MILES | | |
| 1 | .1 | .8 | 1.6 | 2.4 | 3.2 | 3.9 | 4.7 | 5.5 | 6.3 | 7.0 | 7.8 | |
| 0 | 189.00* | I | I | I | I | I | I | I | I | I | I | 185.0 .1 |
| | I | I | I | I | I | I | I | I | I | I | I | |

1111.0 0.0

183.00 1.0
175.00 *
150.00
151.00 1.0
143.00
135.00 3.0
111.0 4.0

183.00 1.0
175.00 *
150.00
151.00 1.0
143.00
135.00 3.0
111.0 4.0

183.00 1.0
175.00 *
150.00
151.00 1.0
143.00
135.00 3.0
111.0 4.0

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183.00 1.0
175.00 *
150.00
151.00 1.0
143.00
135.00 3.0
111.0 4.0

75.00 1.0
.1 .0 1.6 2.4 3.2 3.0 4.7 5.5 6.3 7.0 7.8 7.5.0 7.8

| CROSS-SECTION NO. | MILE | BOTTOM ELEVATION FEET | REACH NO. | REACH LENGTH MILES | SLOPE FT/MI | MESSAGE |
|-------------------|------|-----------------------|-----------|--------------------|-------------|---------|
| 1 | .05 | 189.00 | | | | |
| 1 | .50 | 183.00 | 1 | .45 | 13.33 | |
| 3 | 1.00 | 175.00 | 2 | .50 | 16.00 | |
| 4 | 1.50 | 156.00 | 3 | .50 | 36.00 | |
| 5 | 2.00 | 151.00 | 4 | .50 | 10.00 | |
| 6 | 3.00 | 143.00 | 5 | 1.00 | 8.00 | |
| 7 | 4.00 | 135.00 | 6 | 1.00 | 8.00 | |
| 8 | 5.00 | 111.00 | 7 | 2.00 | 12.00 | |
| 9 | 7.80 | 75.00 | 8 | 1.80 | 20.00 | |

TOTAL NUMBER OF CROSS SECTIONS (ORIGINAL+INTERPOLATED) (N) = 53 MAXIMUM ALLOWABLE = 200

TOTAL VOLUME IN RESERVOIR BEHIND
MENDUMS POND DAM = 3531.3 ACRE-FEET

DEFINITION OF VARIABLES IN RESERVOIR DEPLETION TABLE

| PARAMETER | UNITS | VARIABLE |
|-----------|-------|----------|
| ***** | ***** | ***** |

TIME STEP FROM START OF ANALYSIS

I

ITERATIONS NECESSARY TO SOLVE FLOW EQUATIONS

K

ELAPSED TIME FROM START OF ANALYSIS

HRS TTP/I

TOTAL OUTFLOW FROM DAM

CFS Q/I

ELEVATION OF WATER SURFACE AT DAM

FT H2

ELEVATION OF BOTTOM OF BREACH

FT VB

EST DEPTH OF FLOW IMMEDIATELY DOWNSTREAM

FT D

SUBMERGENCE COEFFICIENT

SUB

VELOCITY CORRECTION

VCOR

TOTAL VOLUME DISCHARGED FROM TIME OF BREACH AC-FT OUTVOL

RECTANGULAR BREACH DISCHARGE COEFFICIENT

INFLOW TO RESERVOIR

COFF

CFS QI(I)

BREACH OUTFLOW

CFS QBRECH

SPILLWAY OUTFLOW

CFS QSPIL

1

RESERVOIR DEPLETION TABLE

| I | K | TTP(I) | Q(I) | H2 | YE | D | SUB | VCOR | OUTVOL | EE | COFR | QI'(I) | QBRECH | QSPIL |
|-----|----|--------|-------|--------|--------|--------|------|------|--------|-----|------|--------|--------|-------|
| *** | ** | ***** | ***** | ***** | ***** | **** | *** | **** | ***** | *** | *** | ***** | ***** | ***** |
| 1 | 0 | 0.000 | 800 | 223.00 | 223.00 | 193.74 | 1.00 | 1.00 | 0.0 | 0.0 | 0.10 | 0.75. | 0. | 800. |
| 1 | 1 | .020 | 802 | 223.00 | 221.44 | 193.74 | 1.00 | 1.00 | 0.7 | 1.0 | 0.10 | 0.75. | 3. | 800. |
| 1 | 2 | .040 | 814 | 223.00 | 221.86 | 193.78 | 1.00 | 1.00 | 1.7 | 0.0 | 0.10 | 0.75. | 15. | 800. |
| 1 | 3 | .060 | 840 | 223.00 | 221.31 | 193.84 | 1.00 | 1.00 | 4.0 | 0.4 | 0.10 | 0.75. | 41. | 799. |
| 1 | 4 | .080 | 882 | 223.00 | 220.76 | 193.96 | 1.00 | 1.00 | 5.5 | 1.0 | 0.10 | 0.75. | 84. | 799. |
| 1 | 5 | .100 | 944 | 221.00 | 220.20 | 194.12 | 1.00 | 1.00 | 7.0 | 0.0 | 0.10 | 0.75. | 146. | 798. |
| 1 | 6 | .120 | 1028 | 221.00 | 219.54 | 194.32 | 1.00 | 1.00 | 8.4 | 0.0 | 0.10 | 0.75. | 131. | 798. |
| 1 | 7 | .140 | 1136 | 221.00 | 219.06 | 194.57 | 1.00 | 1.00 | 10.4 | 1.6 | 0.10 | 0.75. | 326. | 797. |
| 1 | 8 | .160 | 1269 | 221.00 | 218.51 | 194.80 | 1.00 | 1.00 | 11.4 | 1.4 | 0.10 | 0.75. | 473. | 796. |
| 1 | 9 | .180 | 1429 | 221.98 | 217.96 | 195.19 | 1.00 | 1.00 | 14.0 | 1.1 | 0.10 | 0.75. | 625. | 795. |
| 1 | 10 | .200 | 1618 | 221.98 | 217.40 | 195.55 | 1.00 | 1.00 | 17.1 | 1.0 | 0.10 | 0.75. | 825. | 794. |
| 1 | 11 | .220 | 1837 | 222.97 | 216.84 | 195.94 | 1.00 | 1.00 | 20.0 | 0.8 | 0.10 | 0.75. | 1046. | 792. |
| 1 | 12 | .240 | 2088 | 222.96 | 216.28 | 196.36 | 1.00 | 1.00 | 23.0 | 1.0 | 0.10 | 0.75. | 1205. | 795. |
| 1 | 13 | .260 | 2370 | 221.95 | 215.71 | 196.74 | 1.00 | 1.00 | 26.0 | 1.4 | 0.10 | 0.75. | 1584. | 787. |
| 1 | 14 | .280 | 2686 | 222.94 | 215.16 | 197.26 | 1.00 | 1.00 | 31.1 | 1.1 | 0.10 | 0.75. | 1904. | 753. |
| 1 | 15 | .300 | 3037 | 222.93 | 214.60 | 197.81 | 1.00 | 1.00 | 35.0 | 1.0 | 0.10 | 0.75. | 2256. | 779. |
| 1 | 16 | .320 | 3423 | 221.01 | 214.04 | 198.32 | 1.00 | 1.00 | 41.1 | 0.8 | 0.10 | 0.75. | 2649. | 775. |
| 1 | 17 | .340 | 3844 | 221.00 | 213.48 | 198.82 | 1.00 | 1.00 | 47.1 | 0.6 | 0.10 | 0.75. | 3076. | 769. |
| 1 | 18 | .360 | 4303 | 221.00 | 212.91 | 199.32 | 1.00 | 1.00 | 53.0 | 1.4 | 0.10 | 0.75. | 3540. | 763. |
| 1 | 19 | .380 | 4770 | 221.00 | 211.36 | 199.81 | 1.00 | 1.00 | 59.1 | 1.1 | 0.10 | 0.75. | 4041. | 756. |
| 1 | 20 | .400 | 5331 | 221.00 | 211.00 | 200.29 | 1.00 | 1.00 | 65.0 | 0.9 | 0.10 | 0.75. | 4563. | 748. |
| 1 | 21 | .420 | 5901 | 221.00 | 211.14 | 200.77 | 1.00 | 1.00 | 71.1 | 1.0 | 0.10 | 0.75. | 5162. | 740. |

| | | | | | | | | | | | | | | |
|---|----|------|-------|--------|--------|--------|------|------|-------|------|------|-------|--------|------|
| 1 | 1 | .440 | 6510 | 221.76 | 210.68 | 201.25 | 1.00 | 1.00 | 96.3 | 39.6 | 3.10 | 0.75. | 5781. | 730. |
| 1 | 2 | .460 | 7157 | 221.71 | 210.12 | 201.72 | 1.00 | 1.00 | 102.6 | 41.4 | 3.10 | 0.75. | 6438. | 719. |
| 1 | 3 | .480 | 7841 | 221.68 | 209.56 | 201.16 | 1.00 | 1.00 | 113.0 | 43.1 | 3.10 | 0.75. | 7136. | 707. |
| 1 | 4 | .500 | 8565 | 221.67 | 209.02 | 201.62 | 1.00 | 1.00 | 126.0 | 45.0 | 3.10 | 0.75. | 7671. | 693. |
| 1 | 5 | .520 | 9326 | 221.66 | 208.44 | 203.11 | 1.00 | 1.00 | 141.1 | 46.8 | 3.10 | 0.75. | 8048. | 679. |
| 1 | 6 | .540 | 10125 | 221.53 | 207.88 | 203.58 | 1.00 | 1.00 | 157.4 | 48.6 | 3.10 | 0.75. | 9463. | 662. |
| 1 | 7 | .560 | 10962 | 221.47 | 207.32 | 204.04 | 1.00 | 1.00 | 174.6 | 50.4 | 3.10 | 0.75. | 10317. | 645. |
| 1 | 8 | .580 | 11835 | 221.40 | 206.76 | 204.50 | 1.00 | 1.00 | 193.7 | 52.1 | 3.10 | 0.75. | 11209. | 626. |
| 1 | 9 | .600 | 12744 | 221.32 | 206.20 | 204.96 | 1.00 | 1.00 | 214.0 | 54.0 | 3.10 | 0.75. | 12138. | 606. |
| 1 | 10 | .620 | 13688 | 221.24 | 205.64 | 205.35 | 1.00 | 1.00 | 235.0 | 55.8 | 3.10 | 0.75. | 13105. | 584. |
| 1 | 11 | .640 | 14667 | 221.15 | 205.08 | 205.73 | 1.00 | 1.00 | 259.3 | 57.6 | 3.10 | 0.75. | 14107. | 560. |
| 1 | 12 | .660 | 15680 | 221.06 | 204.52 | 206.12 | 1.00 | 1.00 | 284.4 | 59.4 | 3.10 | 0.75. | 15145. | 535. |
| 1 | 13 | .680 | 16724 | 221.96 | 203.96 | 206.52 | 1.00 | 1.00 | 311.2 | 61.2 | 3.10 | 0.75. | 16216. | 508. |
| 1 | 14 | .700 | 17800 | 221.85 | 203.40 | 206.91 | 1.00 | 1.00 | 339.7 | 63.0 | 3.10 | 0.75. | 17320. | 480. |
| 1 | 15 | .720 | 18905 | 221.73 | 201.84 | 207.31 | 1.00 | 1.00 | 370.0 | 64.8 | 3.10 | 0.75. | 18455. | 450. |
| 1 | 16 | .740 | 20037 | 221.60 | 201.26 | 207.71 | 1.00 | 1.00 | 402.2 | 66.6 | 3.10 | 0.75. | 19620. | 418. |
| 1 | 17 | .760 | 21196 | 221.46 | 201.72 | 208.12 | 1.00 | 1.01 | 436.3 | 68.4 | 3.10 | 0.75. | 20811. | 385. |
| 1 | 18 | .780 | 22378 | 221.31 | 201.16 | 208.52 | 1.00 | 1.01 | 472.3 | 70.2 | 3.10 | 0.75. | 22028 | 366. |
| 1 | 19 | .800 | 23582 | 221.15 | 200.48 | 209.71 | -- | -- | -- | -- | -- | 0.75. | -- | -- |

| | | | | | | | | | | | | | | |
|----|---|------|-------|--------|--------|--------|------|------|-------|------|------|------|--------|------|
| 45 | 1 | .000 | 21470 | 216.37 | 198.41 | 210.13 | 1.00 | 1.01 | 636.4 | 77.4 | 3.10 | 675. | 27094. | 200. |
| 46 | 1 | .880 | 28553 | 220.37 | 198.36 | 210.53 | 1.00 | 1.01 | 682.5 | 79.2 | 3.10 | 675. | 28393. | 161. |
| 47 | 1 | .900 | 29818 | 220.14 | 197.80 | 210.82 | 1.00 | 1.01 | 730.8 | 81.0 | 3.10 | 675. | 29697. | 122. |
| 48 | 1 | .920 | 31084 | 219.89 | 197.24 | 211.31 | 1.00 | 1.01 | 781.1 | 82.8 | 3.10 | 675. | 31000. | 84. |
| 49 | 1 | .940 | 32345 | 219.62 | 196.68 | 211.69 | 1.00 | 1.01 | 833.5 | 84.6 | 3.10 | 675. | 32296. | 49. |
| 50 | 1 | .960 | 33592 | 219.33 | 196.12 | 212.07 | 1.00 | 1.02 | 888.0 | 86.4 | 3.10 | 675. | 33573. | 19. |
| | 1 | .980 | 34731 | 219.01 | 195.56 | 212.42 | 1.00 | 1.01 | 944.5 | 88.2 | 3.10 | 675. | 34733. | 0. |

RESERVOIR DEPLETION TABLE

| | K | TTP(I) | Q(I) | H2 | YE | D | SUR | VCOR | OUTVOL | BP | COFR | Q(I)' | QBRECH | QSPIL |
|-----|----|--------|-------|--------|--------|--------|------|------|--------|------|------|-------|--------|-------|
| *** | ** | ***** | ***** | ***** | ***** | ***** | **** | **** | ***** | **** | **** | ***** | ***** | ***** |
| 51 | 1 | 1.000 | 35455 | 218.67 | 195.00 | 210.70 | .00 | 1.00 | 1001.7 | 90.0 | 3.10 | 675. | 35650. | 0. |
| 52 | 1 | 1.020 | 34875 | 218.33 | 195.00 | 211.46 | .00 | 1.01 | 1021.0 | 90.0 | 3.10 | 675. | 34875. | 0. |
| 53 | 1 | 1.040 | 34087 | 217.99 | 195.00 | 212.21 | .00 | 1.02 | 1118.0 | 90.0 | 3.10 | 675. | 34088. | 0. |
| 54 | 1 | 1.060 | 33314 | 217.66 | 195.00 | 211.97 | .00 | 1.01 | 1173.1 | 90.0 | 3.10 | 675. | 33315. | 0. |
| 55 | 1 | 1.080 | 32552 | 217.33 | 195.00 | 211.74 | .00 | 1.01 | 1228.1 | 90.0 | 3.10 | 675. | 32552. | 0. |
| 56 | 1 | 1.100 | 31806 | 217.01 | 195.00 | 211.51 | .00 | 1.01 | 1281.3 | 90.0 | 3.10 | 675. | 31807. | 0. |
| 57 | 1 | 1.120 | 31077 | 216.68 | 195.00 | 211.30 | .00 | 1.01 | 1333.3 | 90.0 | 3.10 | 675. | 31078. | 0. |
| 58 | 1 | 1.140 | 30365 | 216.37 | 195.00 | 211.08 | .00 | 1.00 | 1384.6 | 90.0 | 3.10 | 675. | 30365. | 0. |
| 59 | 1 | 1.160 | 29665 | 216.06 | 195.00 | 210.86 | .00 | 1.01 | 1433.7 | 90.0 | 3.10 | 675. | 29665. | 0. |
| 60 | 1 | 1.180 | 28987 | 215.74 | 195.00 | 210.65 | .00 | 1.00 | 1480.1 | 90.0 | 3.10 | 675. | 28988. | 0. |
| 61 | 1 | 1.200 | 28321 | 215.42 | 195.00 | 210.44 | .00 | 1.01 | 1529.5 | 90.0 | 3.10 | 675. | 28322. | 0. |
| 62 | 1 | 1.220 | 27671 | 215.16 | 195.00 | 210.24 | .00 | 1.02 | 1575.6 | 90.0 | 3.10 | 675. | 27671. | 0. |
| 63 | 1 | 1.240 | 27035 | 214.86 | 195.00 | 210.03 | .00 | 1.01 | 1621.0 | 90.0 | 3.10 | 675. | 27035. | 0. |
| 64 | 1 | 1.260 | 26413 | 214.57 | 195.00 | 209.83 | .00 | 1.00 | 1665.1 | 90.0 | 3.10 | 675. | 26414. | 0. |
| 65 | 1 | 1.280 | 25806 | 214.29 | 195.00 | 209.64 | .00 | 1.00 | 1708.0 | 90.0 | 3.10 | 675. | 25806. | 0. |
| 66 | 1 | 1.300 | 25212 | 214.01 | 195.00 | 209.45 | .00 | 1.00 | 1750.5 | 90.0 | 3.10 | 675. | 25213. | 0. |
| 67 | 1 | 1.320 | 24632 | 213.73 | 195.00 | 209.25 | .00 | 1.02 | 1791.1 | 90.0 | 3.10 | 675. | 24633. | 0. |
| 68 | 1 | 1.340 | 24065 | 213.45 | 195.00 | 209.07 | .00 | 1.02 | 1831.9 | 90.0 | 3.10 | 675. | 24066. | 0. |
| 69 | 1 | 1.360 | 23511 | 213.16 | 195.00 | 208.88 | .00 | 1.02 | 1871.1 | 90.0 | 3.10 | 675. | 23511. | 0. |
| 70 | 1 | 1.380 | 22970 | 212.91 | 195.00 | 208.70 | .00 | 1.02 | 1909.1 | 90.0 | 3.10 | 675. | 22971. | 0. |
| 71 | 1 | 1.400 | 22441 | 212.66 | 195.00 | 208.51 | .00 | 1.02 | 1947.1 | 90.0 | 3.10 | 675. | 22441. | 0. |
| 72 | 1 | 1.420 | 21829 | 212.40 | 195.00 | 208.35 | .00 | 1.02 | 1983.9 | 90.0 | 3.10 | 675. | 21829. | 0. |

| | | | | | | | | | | | | | | |
|----|---|-------|-------|--------|--------|--------|-----|------|--------|------|------|------|--------|----|
| 73 | 1 | 1.440 | 21420 | 212.14 | 195.00 | 208.17 | .00 | 1.02 | 2019.1 | 90.0 | 3.10 | 675. | 21421. | 0. |
| 74 | 1 | 1.460 | 20927 | 211.89 | 195.00 | 208.00 | .00 | 1.02 | 2054.1 | 90.0 | 3.10 | 675. | 20926. | 0. |
| 75 | 1 | 1.480 | 20446 | 211.65 | 195.00 | 207.94 | .00 | 1.02 | 2088.0 | 90.0 | 3.10 | 675. | 20446. | 0. |
| 76 | 1 | 1.500 | 19975 | 211.40 | 195.00 | 207.87 | .00 | 1.04 | 2121.1 | 90.0 | 3.10 | 675. | 19976. | 0. |
| 77 | 1 | 1.520 | 19516 | 211.16 | 195.00 | 207.51 | .00 | 1.04 | 2154.9 | 90.0 | 3.10 | 675. | 19517. | 0. |
| 78 | 1 | 1.540 | 19068 | 210.93 | 195.00 | 207.35 | .00 | 1.04 | 2186.8 | 90.0 | 3.10 | 675. | 19068. | 0. |
| 79 | 1 | 1.560 | 18629 | 210.69 | 195.00 | 207.10 | .00 | 1.04 | 2218.0 | 90.0 | 3.10 | 675. | 18630. | 0. |
| 80 | 1 | 1.580 | 18201 | 210.46 | 195.00 | 207.04 | .00 | 1.04 | 2248.4 | 90.0 | 3.10 | 675. | 18202. | 0. |
| 81 | 1 | 1.600 | 17783 | 210.24 | 195.00 | 206.99 | .00 | 1.04 | 2278.1 | 90.0 | 3.10 | 675. | 17784. | 0. |
| 82 | 1 | 1.620 | 17374 | 210.02 | 195.00 | 206.74 | .00 | 1.04 | 2307.1 | 90.0 | 3.10 | 675. | 17375. | 0. |
| 83 | 1 | 1.640 | 16975 | 209.80 | 195.00 | 206.59 | .00 | 1.05 | 2335.0 | 90.0 | 3.10 | 675. | 16975. | 0. |
| 84 | 1 | 1.660 | 16585 | 209.58 | 195.00 | 206.44 | .00 | 1.05 | 2363.3 | 90.0 | 3.10 | 675. | 16585. | 0. |
| 85 | 1 | 1.680 | 16203 | 209.37 | 195.00 | 206.30 | .00 | 1.05 | 2390.4 | 90.0 | 3.10 | 675. | 16204. | 0. |
| 86 | 1 | 1.700 | 15830 | 209.16 | 195.00 | 206.16 | .00 | 1.05 | 2416.9 | 90.0 | 3.10 | 675. | 15831. | 0. |
| 87 | 1 | 1.720 | 15466 | 208.95 | 195.00 | 206.02 | .00 | 1.05 | 2442.8 | 90.0 | 3.10 | 675. | 15466. | 0. |
| 88 | 1 | 1.740 | 15110 | 208.75 | 195.00 | 205.88 | .00 | 1.05 | 2468.0 | 90.0 | 3.10 | 675. | 15110. | 0. |
| 89 | 1 | 1.760 | 14762 | 208.55 | 195.00 | 205.75 | .00 | 1.05 | 2492.7 | 90.0 | 3.10 | 675. | 14763. | 0. |
| 90 | 1 | 1.780 | 14422 | 208.36 | 195.00 | 205.61 | .00 | 1.06 | 2516.8 | 90.0 | 3.10 | 675. | 14423. | 0. |
| 91 | 1 | 1.800 | 14090 | 208.16 | 195.00 | 205.48 | .00 | 1.06 | 2540.4 | 90.0 | 3.10 | 675. | 14090. | 0. |

| | | | | | | | | | | | | | | |
|-----|---|-------|-------|--------|--------|--------|-----|------|--------|------|------|------|--------|----|
| 103 | 1 | 1.840 | 13448 | 207.79 | 195.00 | 205.23 | .94 | 1.00 | 2525.9 | 90.0 | 3.10 | 675. | 13449. | 0. |
| 104 | 1 | 1.860 | 12138 | 207.60 | 195.00 | 205.10 | .94 | 1.00 | 2607.9 | 90.0 | 3.10 | 675. | 12139. | 0. |
| 105 | 1 | 1.880 | 12838 | 207.42 | 195.00 | 204.98 | .93 | 1.00 | 2629.4 | 90.0 | 3.10 | 675. | 12836. | 0. |
| 106 | 1 | 1.900 | 12562 | 207.24 | 195.00 | 204.84 | .93 | 1.00 | 2650.3 | 90.0 | 3.10 | 675. | 12562. | 0. |
| 107 | 1 | 1.920 | 12296 | 207.07 | 195.00 | 204.71 | .93 | 1.00 | 2670.9 | 90.0 | 3.10 | 675. | 12297. | 0. |
| 108 | 1 | 1.940 | 12038 | 206.89 | 195.00 | 204.58 | .93 | 1.00 | 2691.0 | 90.0 | 3.10 | 675. | 12038. | 0. |
| 109 | 1 | 1.960 | 11785 | 206.71 | 195.00 | 204.45 | .93 | 1.00 | 2710.7 | 90.0 | 3.10 | 675. | 11786. | 0. |
| 110 | 1 | 1.980 | 11539 | 206.56 | 195.00 | 204.32 | .93 | 1.00 | 2730.0 | 90.0 | 3.10 | 675. | 11540. | 0. |

RESERVOIR DEPLETION TABLE

| I | K | TTP(I) | Q(I) | H1 | VR | D | SUB | VCCR | OUTVOL | RR | CORR | QI(I) | QRECH | OSPI |
|-----|----|--------|-------|--------|--------|--------|------|-------|--------|------|------|-------|--------|-------|
| *** | ** | ***** | ***** | ***** | ***** | ***** | **** | ***** | ***** | **** | **** | ***** | ***** | ***** |
| 101 | 1 | 1.000 | 11098 | 206.39 | 195.00 | 204.20 | .93 | 1.00 | 2745.9 | 90.0 | 3.10 | 675. | 11099. | 0. |
| 102 | 1 | 1.020 | 11063 | 206.23 | 195.00 | 204.07 | .93 | 1.00 | 2767.3 | 90.0 | 3.10 | 675. | 11064. | 0. |
| 103 | 1 | 1.040 | 10819 | 206.05 | 195.00 | 203.94 | .93 | 1.00 | 2787.2 | 90.0 | 3.10 | 675. | 10820. | 0. |
| 104 | 1 | 1.060 | 10549 | 205.84 | 195.00 | 203.79 | .92 | 1.00 | 2805.6 | 90.0 | 3.10 | 675. | 10550. | 0. |
| 105 | 1 | 1.083 | 10261 | 205.65 | 195.00 | 203.63 | .92 | 1.00 | 2831.9 | 90.0 | 3.10 | 675. | 10262. | 0. |
| 106 | 1 | 1.102 | 9955 | 205.43 | 195.00 | 203.46 | .92 | 1.00 | 2855.6 | 90.0 | 3.10 | 675. | 9956. | 0. |
| 107 | 1 | 1.114 | 9632 | 205.14 | 195.00 | 203.28 | .91 | 1.00 | 2881.0 | 90.0 | 3.10 | 675. | 9633. | 0. |
| 108 | 1 | 1.119 | 6201 | 204.94 | 195.00 | 203.08 | .91 | 1.00 | 2905.7 | 90.0 | 3.10 | 675. | 6202. | 0. |
| 109 | 1 | 1.120 | 2834 | 204.80 | 195.00 | 201.86 | .91 | 1.00 | 2939.1 | 90.0 | 3.10 | 675. | 2835. | 0. |
| 110 | 1 | 1.121 | 851 | 204.67 | 195.00 | 201.69 | .90 | 1.00 | 2970.1 | 90.0 | 3.10 | 675. | 8561. | 0. |
| 111 | 1 | 1.131 | 8174 | 204.05 | 195.00 | 201.36 | .91 | 1.00 | 3002.7 | 90.0 | 3.10 | 675. | 8174. | 0. |
| 112 | 1 | 1.137 | 7773 | 203.73 | 195.00 | 201.12 | .91 | 1.00 | 3036.0 | 90.0 | 3.10 | 675. | 7774. | 0. |
| 113 | 1 | 1.142 | 7362 | 203.58 | 195.00 | 201.85 | .91 | 1.00 | 3071.5 | 90.0 | 3.10 | 675. | 7361. | 0. |
| 114 | 1 | 1.149 | 6941 | 203.01 | 195.00 | 201.55 | .91 | 1.00 | 3106.7 | 90.0 | 3.10 | 675. | 6941. | 0. |
| 115 | 1 | 1.159 | 6515 | 202.81 | 195.00 | 201.23 | .91 | 1.00 | 3146.1 | 90.0 | 3.10 | 675. | 6515. | 0. |
| 116 | 1 | 1.163 | 6086 | 202.21 | 195.00 | 200.90 | .91 | 1.00 | 3187.6 | 90.0 | 3.10 | 675. | 6087. | 0. |
| 117 | 1 | 1.170 | 5661 | 201.76 | 195.00 | 200.56 | .91 | 1.00 | 3228.1 | 90.0 | 3.10 | 675. | 5661. | 0. |
| 118 | 1 | 1.181 | 5243 | 201.35 | 195.00 | 200.20 | .91 | 1.00 | 3269.6 | 90.0 | 3.10 | 675. | 5243. | 0. |
| 119 | 1 | 1.191 | 4838 | 200.90 | 195.00 | 199.83 | .91 | 1.00 | 3311.7 | 90.0 | 3.10 | 675. | 4837. | 0. |
| 120 | 1 | 1.203 | 4446 | 200.49 | 195.00 | 199.45 | .91 | 1.00 | 3354.3 | 90.0 | 3.10 | 675. | 4447. | 0. |
| 121 | 1 | 1.215 | 4078 | 199.96 | 195.00 | 199.07 | .90 | 1.00 | 3397.4 | 90.0 | 3.10 | 675. | 4078. | 0. |
| 122 | 1 | 1.220 | 3732 | 199.47 | 195.00 | 198.70 | .90 | 1.00 | 3440.9 | 90.0 | 3.10 | 675. | 3733. | 0. |

| | | | | | | | | | | | | | | |
|-----|---|--------|------|--------|--------|--------|------|------|--------|------|------|------|-------|----|
| 123 | 1 | 3.428 | 3428 | 198.97 | 195.00 | 198.21 | .88 | 1.00 | 3484.8 | 90.0 | 3.10 | 675. | 3421. | 0. |
| 124 | 1 | 3.501 | 3223 | 198.46 | 195.00 | 197.93 | .85 | 1.00 | 3528.6 | 90.0 | 3.10 | 675. | 3123. | 0. |
| 125 | 1 | 3.570 | 1731 | 197.94 | 195.00 | 197.34 | .85 | 1.00 | 3572.0 | 90.0 | 3.10 | 675. | 1733. | 0. |
| 126 | 1 | 3.647 | 1124 | 197.50 | 195.00 | 196.57 | 1.00 | 1.00 | 3612.2 | 90.0 | 3.10 | 675. | 2226. | 0. |
| 127 | 1 | 4.164 | 1735 | 197.12 | 195.00 | 195.76 | 1.00 | 1.00 | 3647.8 | 90.0 | 3.10 | 675. | 1735. | 0. |
| 128 | 1 | 4.422 | 1387 | 196.82 | 195.00 | 195.10 | 1.00 | 1.00 | 3678.6 | 90.0 | 3.10 | 675. | 1388. | 0. |
| 129 | 1 | 4.684 | 1144 | 196.51 | 195.00 | 194.59 | 1.00 | 1.00 | 3708.0 | 90.0 | 3.10 | 675. | 1145. | 0. |
| 130 | 1 | 4.973 | 977 | 196.45 | 195.00 | 194.20 | 1.00 | 1.00 | 3731.3 | 90.0 | 3.10 | 675. | 978. | 0. |
| 131 | 1 | 5.290 | 964 | 196.33 | 195.00 | 193.91 | 1.00 | 1.00 | 3755.5 | 90.0 | 3.10 | 675. | 965. | 0. |
| 132 | 1 | 5.639 | 785 | 196.26 | 195.00 | 193.71 | 1.00 | 1.00 | 3779.3 | 90.0 | 3.10 | 675. | 790. | 0. |
| 133 | 1 | 6.023 | 741 | 196.20 | 195.00 | 193.57 | 1.00 | 1.00 | 3803.0 | 90.0 | 3.10 | 675. | 741. | 0. |
| 134 | 1 | 6.445 | 712 | 196.17 | 195.00 | 193.49 | 1.00 | 1.00 | 3829.0 | 90.0 | 3.10 | 675. | 712. | 0. |
| 135 | 1 | 6.910 | 694 | 196.15 | 195.00 | 193.43 | 1.00 | 1.00 | 3856.0 | 90.0 | 3.10 | 675. | 694. | 0. |
| 136 | 1 | 7.420 | 684 | 196.14 | 195.00 | 193.36 | 1.00 | 1.00 | 3885.1 | 90.0 | 3.10 | 675. | 684. | 0. |
| 137 | 1 | 7.983 | 679 | 196.14 | 195.00 | 193.38 | 1.00 | 1.00 | 3916.8 | 90.0 | 3.10 | 675. | 679. | 0. |
| 138 | 1 | 8.601 | 676 | 196.13 | 195.00 | 193.37 | 1.00 | 1.00 | 3951.4 | 90.0 | 3.10 | 675. | 677. | 0. |
| 139 | 1 | 9.281 | 675 | 196.13 | 195.00 | 193.37 | 1.00 | 1.00 | 3989.4 | 90.0 | 3.10 | 675. | 676. | 0. |
| 140 | 1 | 10.029 | 675 | 196.13 | 195.00 | 193.38 | 1.00 | 1.00 | 4031.1 | 90.0 | 3.10 | 675. | 675. | 0. |

| PARAMETER | UNITS | VARIABLE | VALUE |
|--|-------|----------|--------|
| INITIAL FLOW | CFS | Q(1) | 822. |
| MAX FLOW | CFS | QM | 35±5c. |
| FINAL FLOW | CFS | Q(NU) | c7E. |
| TIME TO MAX FLOW | HRS | TP | 1.22 |
| NUMBER OF TIME STEPS | NNU | | 142 |
| TOTAL VOLUME DISCHARGED FROM RESERVOIR | AC-FT | DISVOL | 4231. |

| | | |
|---------------------------------|--------|-----|
| NUMBER OF INTERMEDIATE STATIONS | NN(NS) | 52 |
| NUMBER OF TIME STEPS | NNU | 1-2 |

B-15
TIME PARAMETERS OF OUTFLOW HYDROGRAPH IMMEDIATELY DOWNSTREAM OF DAM

| PARAMETER | UNITS | VARIABLE | VALUE |
|--|-------|----------|-------|
| TIME TO FAILURE | HR | TF1 | 1.222 |
| TIME TO START OF RISING LIME OF HYDROGRAPH | HR | TFO | 0.222 |

| | | | |
|----------------|----|------|-------|
| TIME TO PEAK | HR | TP | 1.222 |
| TIME STEP SIZE | HR | DTHI | 2E-2 |

NONCONVERGENCE OCCURRED AT CROSS-SECT 34 AND . 35 36 37 38 39 40 41 42 43
 $TT=$ 2.890 $\Delta T=$.028 $ITERR=$ 9

KTIME=141

ALLOWABLE KTIME= 698

TT= 10.0

PROFILE OF CRESTS AND TIMES FOR MENDUM POND
BELOW MENDUM POND DAM

| RVR MILE FROM DAM | MAX ELEV (FT) | MAX FLOW (CFS) | TIME MAX ELEV(HR) | MAX VEL (FT/SEC) | MAX VEL (MI/HR) | FLOOD ELEV (FT) | TIME FLOOD ELEV (HR) |
|----------------------|------------------|-------------------|----------------------|---------------------|--------------------|--------------------|-------------------------|
| ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** |
| .050 | 210.03 | 35655 | 1.000 | 5.48 | 3.77 | 0.00 | 0.00 |
| .100 | 208.33 | 34713 | 1.050 | 5.29 | 3.60 | 0.00 | 0.00 |
| .175 | 206.46 | 33996 | 1.050 | 5.04 | 3.43 | 0.00 | 0.00 |
| .300 | 204.56 | 33410 | 1.100 | 5.08 | 3.46 | 0.00 | 0.00 |
| .500 | 202.29 | 32753 | 1.100 | 5.26 | 3.58 | 0.00 | 0.00 |
| .500 | 200.14 | 32479 | 1.150 | 5.39 | 3.58 | 0.00 | 0.00 |
| .700 | 197.96 | 31958 | 1.150 | 5.45 | 3.71 | 0.00 | 0.00 |
| .800 | 195.70 | 31827 | 1.200 | 5.75 | 3.64 | 0.00 | 0.00 |
| .900 | 193.12 | 31493 | 1.200 | 5.21 | 4.74 | 0.00 | 0.00 |
| 1.000 | 189.59 | 31458 | 1.300 | 7.80 | 11.18 | 0.00 | 0.00 |
| 1.100 | 185.72 | 31296 | 1.350 | 7.30 | 4.98 | 0.00 | 0.00 |
| 1.200 | 181.87 | 31221 | 1.350 | 7.00 | 4.17 | 0.00 | 0.00 |
| 1.300 | 178.20 | 31083 | 1.300 | 8.67 | 4.55 | 0.00 | 0.00 |
| 1.400 | 175.39 | 30695 | 1.350 | 5.81 | 5.83 | 0.00 | 0.00 |
| 1.500 | 173.96 | 30175 | 1.400 | 4.04 | 2.74 | 0.00 | 0.00 |
| 1.600 | 172.75 | 29558 | 1.450 | 4.04 | 2.76 | 0.00 | 0.00 |
| 1.700 | 171.64 | 28948 | 1.500 | 4.03 | 2.75 | 0.00 | 0.00 |
| 1.800 | 170.51 | 28455 | 1.550 | 4.11 | 2.80 | 0.00 | 0.00 |
| 1.900 | 169.42 | 27892 | 1.650 | 4.07 | 2.78 | 0.00 | 0.00 |
| 2.000 | 168.38 | 27547 | 1.600 | 4.03 | 2.75 | 0.00 | 0.00 |
| 2.100 | 167.28 | 28296 | 1.600 | 4.20 | 2.84 | 0.00 | 0.00 |
| 2.200 | 166.20 | 27925 | 1.650 | 4.13 | 2.81 | 0.00 | 0.00 |
| 2.300 | 165.13 | 27556 | 1.650 | 4.07 | 2.77 | 0.00 | 0.00 |
| 2.400 | 164.08 | 27236 | 1.700 | 4.08 | 2.78 | 0.00 | 0.00 |
| 2.500 | 163.01 | 26914 | 1.700 | 4.04 | 2.75 | 0.00 | 0.00 |
| 2.600 | 161.94 | 26580 | 1.750 | 4.06 | 2.76 | 0.00 | 0.00 |
| 2.700 | 160.81 | 26314 | 1.800 | 4.09 | 2.79 | 0.00 | 0.00 |
| 2.800 | 159.67 | 25998 | 1.800 | 4.13 | 2.82 | 0.00 | 0.00 |
| 2.900 | 158.44 | 25737 | 1.850 | 4.30 | 2.93 | 0.00 | 0.00 |
| 3.000 | 157.15 | 25394 | 2.000 | 4.50 | 3.07 | 0.00 | 0.00 |
| 3.167 | 156.21 | 24787 | 2.000 | 4.43 | 3.01 | 0.00 | 0.00 |
| 3.333 | 155.30 | 25179 | 1.950 | 4.40 | 3.00 | 0.00 | 0.00 |
| 3.500 | 154.35 | 23936 | 1.950 | 4.34 | 2.98 | 0.00 | 0.00 |
| 3.667 | 152.94 | 25868 | 1.950 | 4.27 | 2.91 | 0.00 | 0.00 |
| 3.833 | 151.80 | 25156 | 1.900 | 4.34 | 2.96 | 0.00 | 0.00 |
| 4.000 | 150.18 | 26618 | 1.900 | 5.02 | 3.42 | 0.00 | 0.00 |
| 4.200 | 147.72 | 26986 | 2.000 | 5.42 | 3.70 | 0.00 | 0.00 |
| 4.400 | 145.77 | 26139 | 1.950 | 4.84 | 3.30 | 0.00 | 0.00 |
| 4.600 | 143.18 | 27201 | 2.150 | 6.06 | 4.13 | 0.00 | 0.00 |
| 4.800 | 141.05 | 25067 | 2.301 | 5.33 | 3.63 | 0.00 | 0.00 |

| | | | | | | | |
|-------|--------|-------|-------|------|------|------|------|
| 5.200 | 136.87 | 22788 | 2.403 | 4.91 | 3.35 | 0.00 | 0.00 |
| 5.400 | 134.77 | 22432 | 2.455 | 4.96 | 3.38 | 0.00 | 0.00 |
| 5.600 | 131.58 | 22103 | 1.508 | 5.03 | 3.43 | 0.00 | 0.00 |
| 5.800 | 130.13 | 22069 | 2.508 | 5.39 | 3.68 | 0.00 | 0.00 |
| 6.000 | 126.27 | 21953 | 2.561 | 7.07 | 4.82 | 0.00 | 0.00 |
| 6.257 | 119.79 | 21840 | 2.614 | 6.92 | 4.72 | 0.00 | 0.00 |
| 6.514 | 113.46 | 21555 | 2.668 | 6.79 | 4.63 | 0.00 | 0.00 |

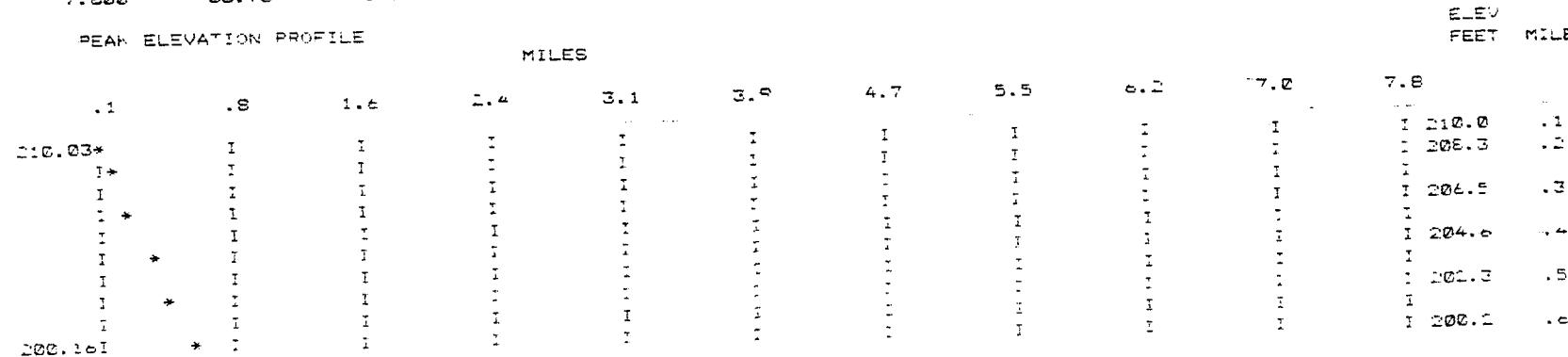
1

PROFILE OF CRESTS AND TIMES FOR MENDUMS POND
BELOW MENDUMS POND DAM

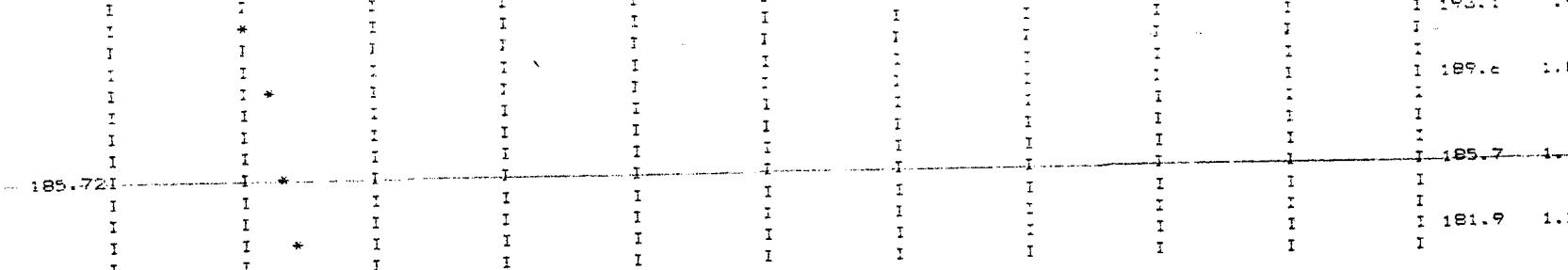
| RVR MILE FROM DAM | MAX ELEV (FT) | MAX FLOW (CFS) | TIME MAX ELEV(HR) | MAX VEL (FT/SEC) | MAX VEL (MI/HR) | FLOOD ELEV (FT) | TIME FLOOD ELEV (HR) |
|----------------------|------------------|-------------------|----------------------|---------------------|--------------------|--------------------|-------------------------|
| ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** |
| 6.771 | 107.30 | 21400 | 1.723 | 6.66 | 4.55 | 0.00 | 0.00 |
| 7.029 | 101.27 | 21040 | 1.834 | 6.57 | 4.48 | 0.00 | 0.00 |
| 7.286 | 95.36 | 20598 | 2.010 | 6.36 | 4.34 | 0.00 | 0.00 |
| 7.543 | 89.40 | 19982 | 1.976 | 6.19 | 4.21 | 0.00 | 0.00 |
| 7.800 | 83.73 | 19386 | 3.093 | 6.04 | 4.11 | 0.00 | 0.00 |

PEAK ELEVATION PROFILE

MILES



200.101



DISCHARGE HYDROGRAPH FOR MENDUME POND
BELOW MENDUME FDNL DAM

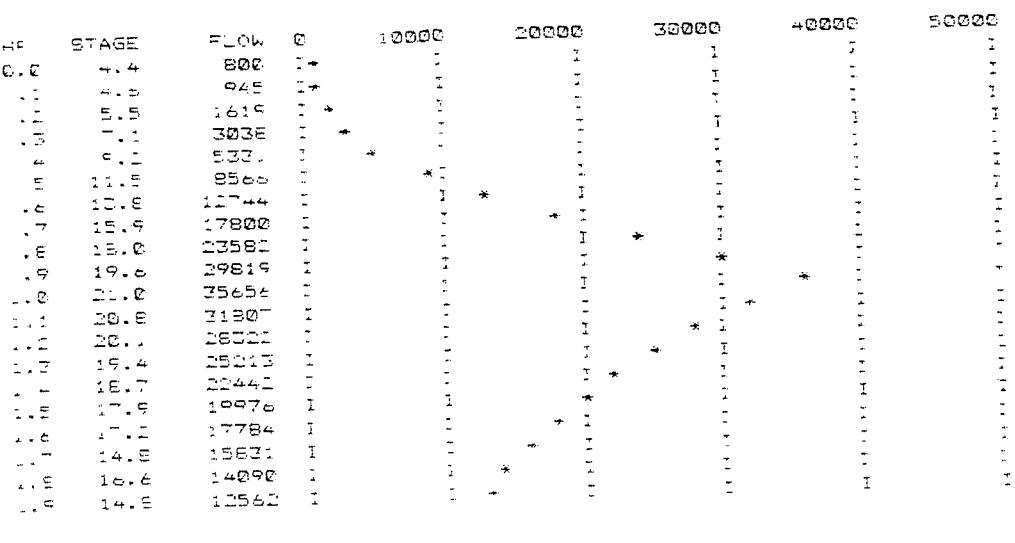
... STATION NUMBER 1
AT MILE .05

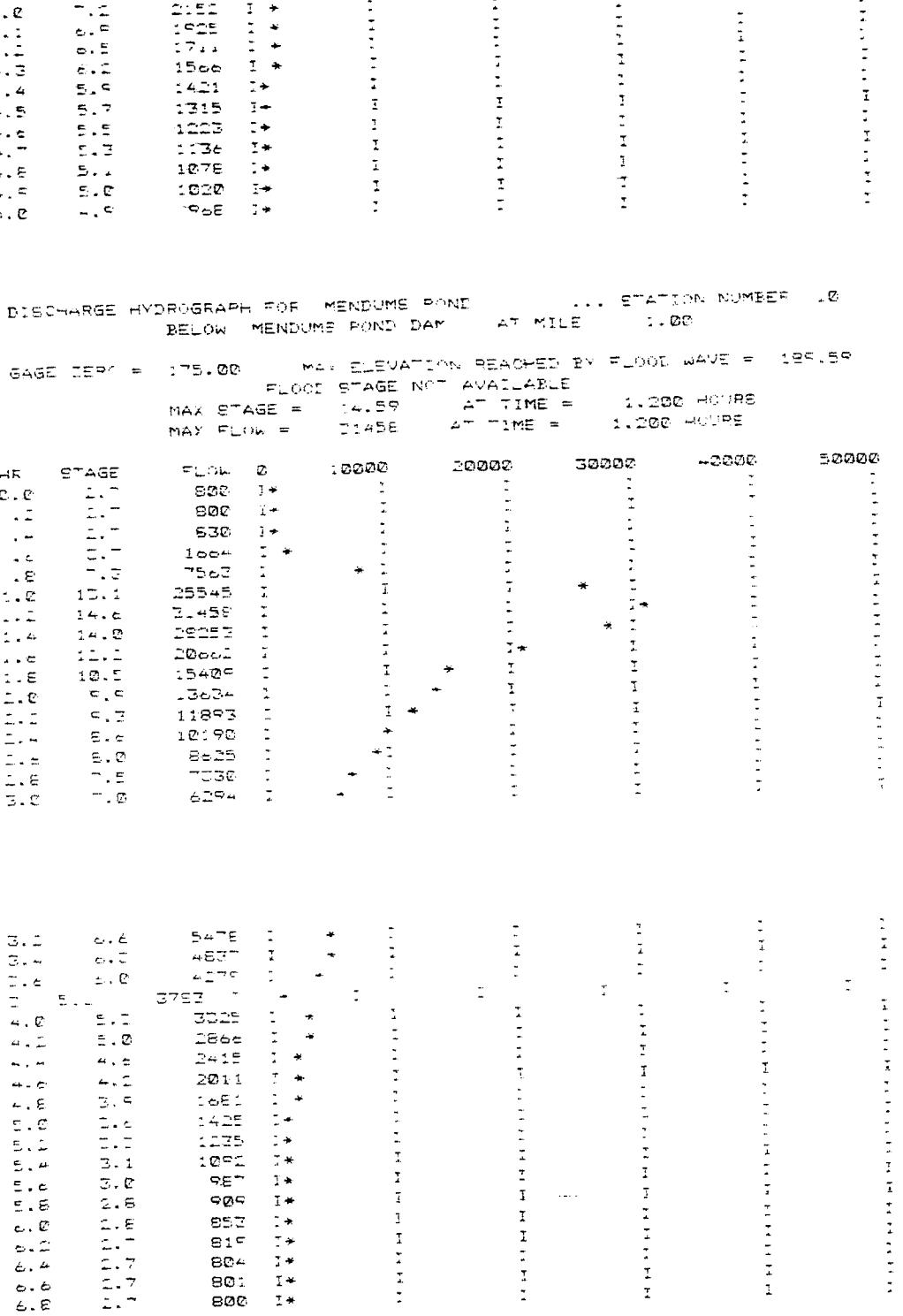
GAGE ZERO = 125.00 MAX ELEVATION REACHED BY FLOOD WAVE = 110.00

FLOOD STAGE NOT AVAILABLE

MAX STAGE = 21.00 AT TIME = 1.000 HOURS

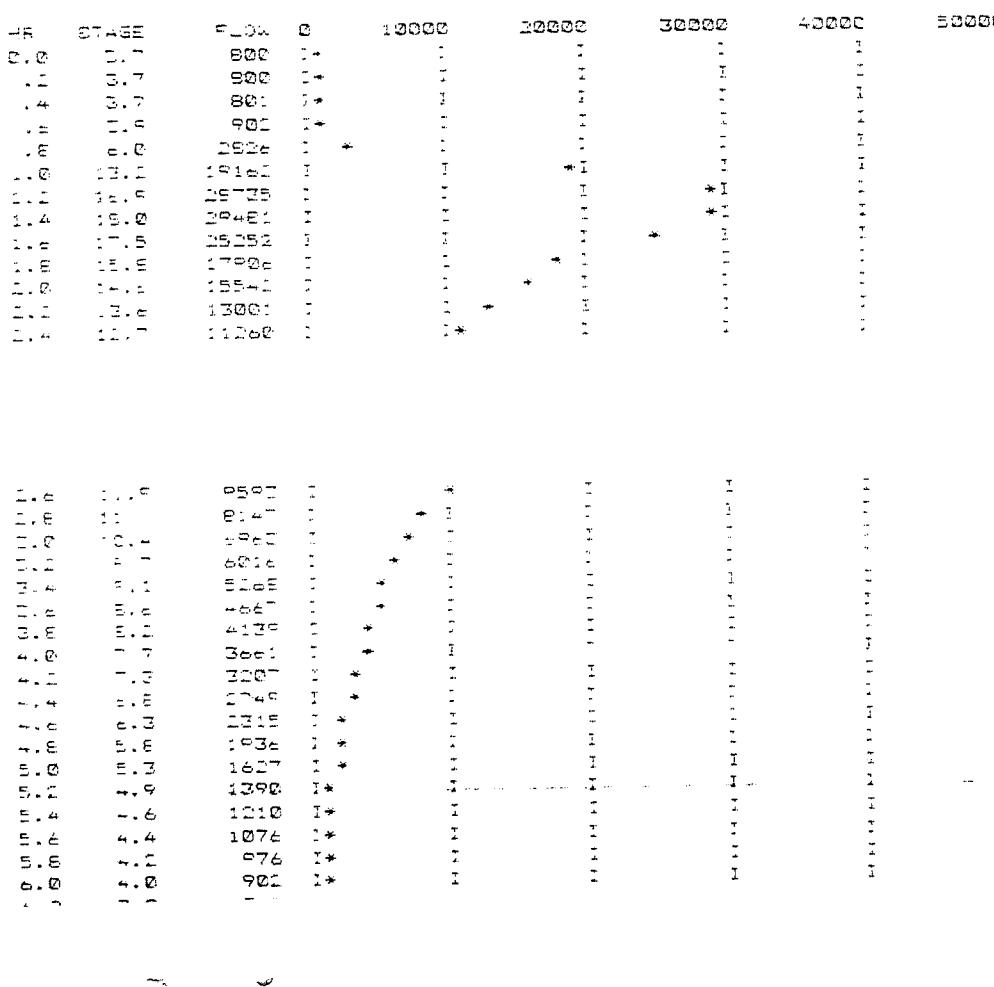
MAX FLOW = 35256 AT TIME = 1.000 HOURS





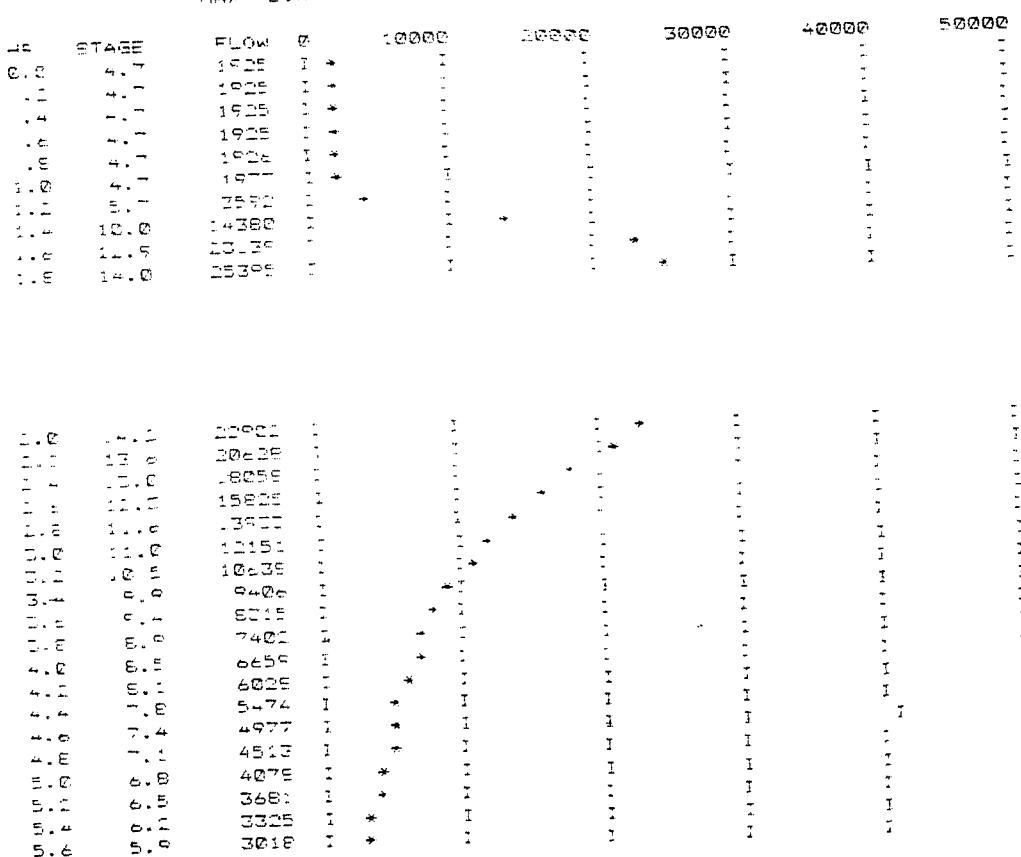
DISCHARGE HYDROGRAPH FOR MENDUMS POND . . . STATION NUMBER 15
BELOW MENDUMS POND DAM AT MILK 1.50

GAGE ELEV = 150.00 MAY ELEVATION REACHED BY FLOOD WAVE = 173.00
FLOOD STAGE NOT AVAILABLE
MAX STAGE = 17.90 TIME = 1.400 HOURS
MAX FLOW = 20170 TIME = 1.300 HOURS



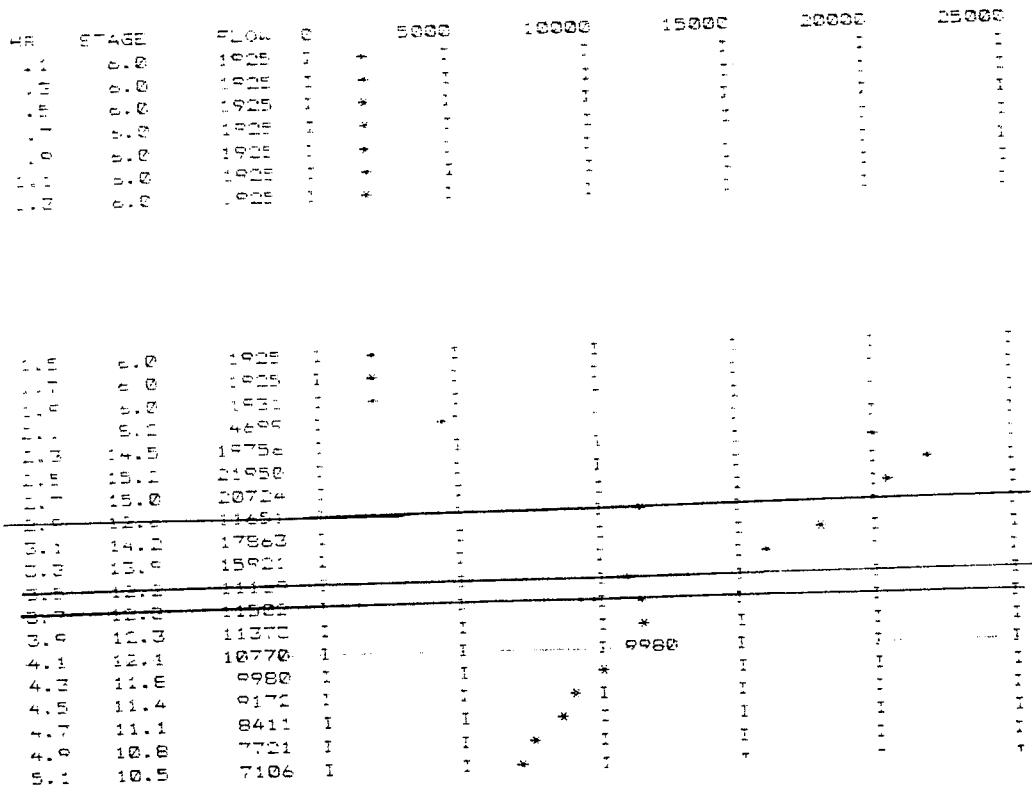
0.0 0.2 0.4 0.6 0.8 1.0 1.2 1.4 1.6 1.8 2.0

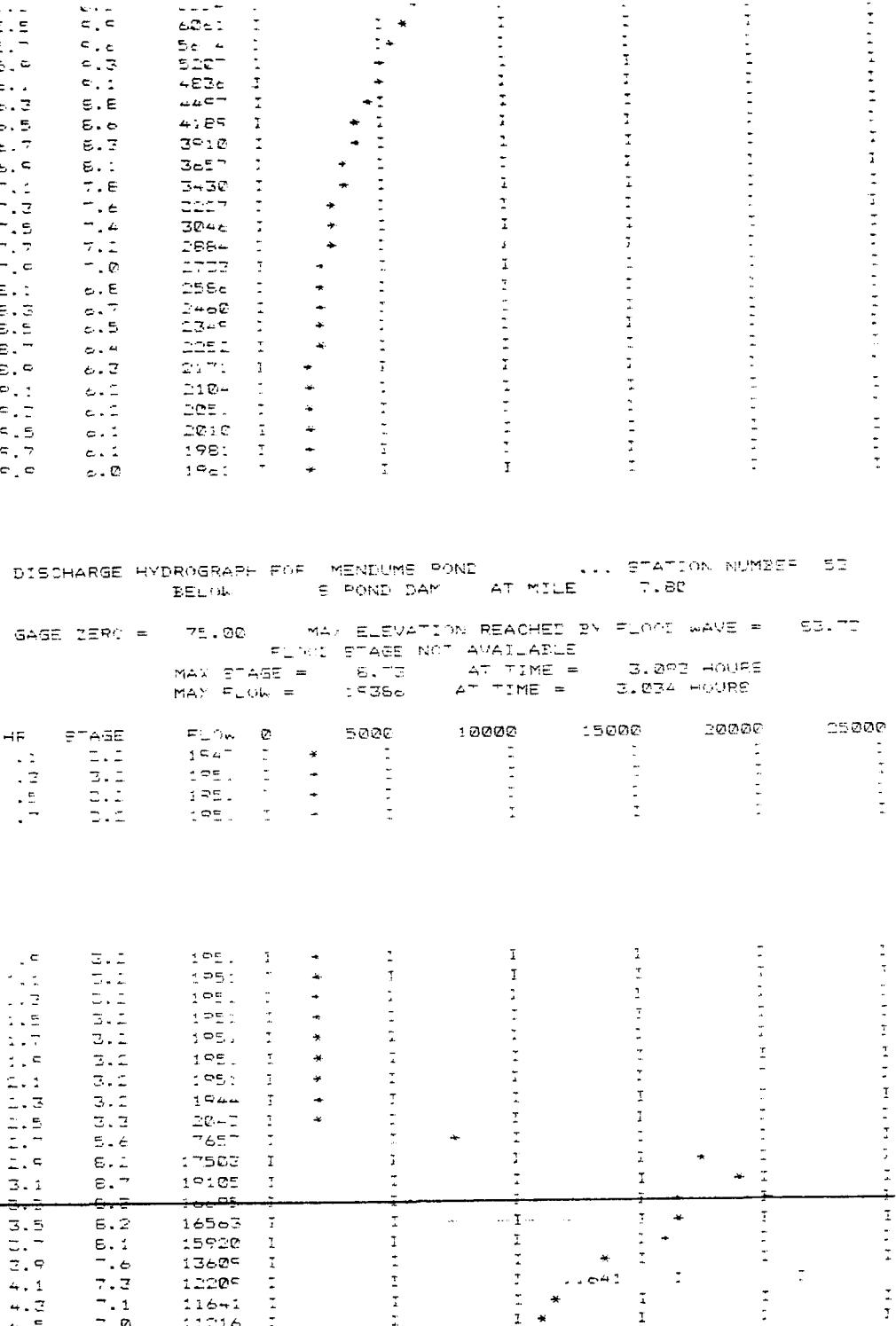
DISCHARGE HYDROGRAPH FOR MENDUM POND
BELOW MENDUM POND DAM AT MILE 0.00
... STATION NUMBER 30
BASE ZERO = 145.00 MAX ELEVATION REACHED BY FLOOD WATERS = 167.16
STAGE NOT AVAILABLE
MAX STAGE = 14.00 AT TIME = 1.000 HOUR
MAX FLOW = 26700 AT TIME = 1.500 HOUR



DISCHARGE HYDROGRAPH FOR MENDOME RIVER
BELOW MENDOME RIVER DAM 4 MILE 0.60
... STATION NUMBER 40

GAGE ZERO = 111.00 MAX ELEVATION REACHED BY FLOOD WAVE = 126.27
 FLOOD STAGE NOT AVAILABLE
 MAX STAGE = 116.07 AT TIME = 1.561 HOURS
 MAX FLOW = 21,000 FT³/SEC AT TIME = 1.561 HOURS





READY,
LOGOUT

2384682 LOG OFF ID = 15951.
SBIAF CME 00.20. LOGGED OUTIAF
LOGGED OUT.
**

CONNECT TIME 00.16.48.